

SUPPLEMENTAL DATA REPORT

# **Proposed Age Restricted Housing Development**

# 797 Boston Road

Groton, Massachusetts

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# **Existing Conditions**

The subject site is located at 797 Boston Road in Groton, MA. The site consists of one corner parcel totaling 117,594 square feet (2.7 acres). The subject site is located within the Residential-Agricultural zoning district and the Water Resources Protection Overlay District III, located at the signalized intersection of Forge Village Road (Route 225) and Boston Road (Route 119) in Groton. Residential abutters, commercial spaces, and small businesses surround this property on all sides.

The existing topography has a 1-5% grade sloping from northwest to the east and southeast, with elevations ranging from 269 to 260 feet, allowing runoff to cultivate on the southeast side of the property. The property previously had a wooden barn with gravel access from both Boston Road and Forge Village Road. This barn has since been removed and has gravel sections and remnants of where the structure used to remain on the site. The property is primarily cleared of trees except for a small section of woods near the intersection of Forge and Boston Road and adjacent to the residential abutters to the east.

The site has soil categorized as Quonset Sandy Loam, corresponding to Hydrologic Group A. Soil testing conducted on site confirms this soil type. The existing property has no impervious surfaces other than the remaining gravel sections and a small section of concrete which is to be removed. Additionally, the site does not feature any stormwater treatment and most of the site flows downhill towards an existing depression onsite adjacent to the eastern abutter.

The existing electricity is overhead, connecting from a utility pole located on Forge Village Road to the north side of the site. The underground water line connection is also from Forge Village Road connecting to the north side of the property. No sewerage connection exists for the site as it is located just outside the sewer district improvements.

The site hydrology is simple with the edge of the watershed starting at the back of the existing sidewalk at the intersection of Forge Village Road and Boston Road and flowing down and across the site to the southeast where it eventually enters the existing depression at the bottom corner of the site prior to overflowing to the eastern abutters downslope denoted as Analysis Point #1 (AP1).

# **Proposed Conditions**

The project calls for the construction of two-twelve (12) unit age restricted housing buildings with associated parking, utilities, drainage, and amenities. The project is comprised of two, two-story buildings, each with 12 one-bedroom units and 12 two-bedroom units. The units are proposed at 50% affordability per the requirements of age restricted housing in Groton. A proposed driveway will be



constructed in a one-way direction entering and exiting onto Forge Village Road (Route 225). Parking and impervious surfaces are increased from the existing condition but remain under the impervious requirements with the addition of porous pavement

The site access is a one-way driveway which will loop off and back onto Forge Village Road (Route 225) in a counterclockwise direction through the parking for the development. The development proposes 36 parking spaces, including 4 accessible spaces, along the driveway near the building entrances located on either side of the parking areas. The proposed impervious surface will increase to 22%± and comply with the Town of Groton requirements. Green space will be created surrounding each of the buildings, with a large open space on the west side of the parcel creating a buffer between the proposed residential units and the existing signalized intersection. The existing wooded areas at the intersection of Boston Road and Forge Village Road will remain intact and the woodland adjacent to the eastern abutters will remain primarily intact with some small adjustment to accommodate the proposed dumpster and parking lot grading to tie back into the existing topography. Pedestrian access will be improved around the site with entryways on the sides and front of the buildings facing the parking lot and driveway. Additionally, sidewalk connections have been proposed along Boston Road and Forge Village Road to improve pedestrian connectivity from this development.

All stormwater onsite is routed and infiltrated into the ground through a single section of porous pavement located through the parking section of the development. The driveway and parking spaces infiltrate through the top of the porous pavement. The stormwater from the roofs of the two buildings flows through roof drains to the subbase of the porous pavement for infiltration into the ground. The site also accepts stormwater from Forge Village Road which flows through a Rain Guardian Foxhole and is collected by a yard drain. There are other yard drains that collect stormwater from grassed areas around the two proposed buildings. All stormwater collected from yard drains is also piped to the subbase of the porous pavement for infiltration. Any potential overflow will be captured via a perforated underdrain overflow within the porous pavement system and be directed towards the existing low point onsite and eventually to Analysis Point #1.

# **Stormwater Management Standards**

# Standard 1: No new untreated discharges

The Massachusetts Stormwater Handbook requires that the project demonstrates that no new stormwater conveyances (e.g. outfalls) discharge untreated stormwater directly to or cause erosion in wetlands or waters of the Commonwealth.

The proposed project will not discharge stormwater directly to, or cause erosion in, wetlands or water of the Commonwealth and will treat stormwater prior to discharge or infiltration.

BMP's have been proposed to treat stormwater collected from the paved areas. The overflow discharges have been designed to outlet to flared end sections with riprap to minimize any erosion. There are no vegetated wetlands present on the site. In the 2-year storm event there is no discharge from the BMPs so the need to determine a stormwater discharge velocity is not applicable.

# Standard 2: Post-development peak discharge rates not to exceed pre-development peak discharge rates.

Post-development peak discharge rates and total runoff volumes do not exceed the pre-development peak discharge rates and total runoff volumes for all storm events. The proposed condition reduces rates by collecting and controlling the stormwater runoff within the porous pavement stormwater management system.

Storm Event	2-year	10-year	25-year	100-year
Pre-Development Rates (cfs) AP1	0.00	2.18	4.49	7.26
Volume (cf)	0.00	3,483	9,576	20,740
Post-Development Rates (cfs) AP1	0.00	0.00	0.28	2.65
Volume (cf)	0.00	0.00	471	4,989
Rate Reductions (cfs)	0.00	-2.18	-4.21	-4.61
Volume Reductions (cf)	0.00	-3,483	-9,105	-15,751

# Standard 3: Minimize or eliminate loss of annual recharge to groundwater.

Groundwater recharge will be accomplished by directing stormwater runoff from impervious surfaces to designed areas of infiltration into the ground. As shown in the table summary for Standard 2, the project decreases the total volume of runoff for all storm events. This reduction in volume is generated by collecting, treating, and infiltrating a significant portion of the proposed impervious surfaces created on site through the porous pavement.

#### Recharge Volume Requirement:

Rv = F x impervious area

Rv = Required Recharge Volume, expressed in Ft<sup>3</sup>, cubic yards, or acre-feet

F= Target Depth Factor associated with each Hydrologic Soil Group

Impervious Area = pavement (including porous sections) and rooftop area



Recharge volume for the entire site:
Soil A:
Rv=0.60 in \* 45,408 sf (see note above) \* 1 ft / 12 in = 2,270 cf recharge
Soil B:
No B soils were found on site.
Soil C:
No C soils were found on site.
Soil D:
No D soils were found on site.
Total recharge required:
Rv= 2,270 cf total recharge required

<u>Total recharge provided:</u> Porous Pavement = 5,185 cf below outlet Existing Site Depression= 4,588 cf below outlet <u>Total site recharge provided = 9,773 cf recharge volume > 2,270 cf required</u>

#### **Drawdown Within 72 Hours**

Porous Pavement: 5,185 cf / [(2.41 in/hr)(1 ft/12 in)(10,986 sf)] = 2.4 hours < 72 hours, OK

Infiltration Basin: 4,588 cf / [(2.41 in/hr)(1 ft/12 in)(2,056 sf)] = 11.1 hours < 72 hours, OK

#### Water Quality Volume

Calculated as Vwq = (Dwq/12 inches/foot) \* (Aimp \* 43,560 square feet/acre), where:

V*wq* = required water quality volume (in cubic feet)

Dwq = water quality depth: one-inch for discharges within a Zone II or Interim Wellhead Protection Area, to or near another critical area, runoff from a LUHPPL, or exfiltration to soils with infiltration rate greater than 2.4 inches/hour or greater;  $\frac{1}{2}$  inch for discharges near or to other areas.

Aimp = impervious area (in sf)

*Aimp* = *Impervious Area of Subcatchments* = 45,408 *sf* 

Dwq = 1 inch

*Vwq* = (1 inch / 12 inches / foot) \* (45,408 sf) = 3,784 cf



#### Total Water Quality Volumes from proposed BMP's = 5,185 cf + 4,588 cf = 9,773 cf

#### 9,773 cf > 3,784 cf OK

#### Porous Pavement:

Porous pavement = (1 inch / 12 inches / foot) \* (44,467 sf) =3,706 cf

Volume provided below outlet = 5,185 cf

5,185 cf > 3,706 cf OK

Infiltration Basin:

Porous pavement = (1 inch / 12 inches / foot) \* (941 sf) = 78 cf

Volume provided below outlet = 4,588 cf

4,588 cf > 78 cf OK

\*This section of impervious sidewalk which flows overland towards the existing infiltration basin is considered clean

Ferguson Rain Guardian Foxhole:

Ferguson Rain Guardian Foxhole rated for 88% removal up to 0.25 cfs Ferguson Rain Guardian Foxhole rated for 79% removal up to 0.50 cfs

Flow rate associated with Ferguson Rain Guardian Foxhole: Q = (qu)\*(A)\*(WQV), where: Q = Peak flow rate associated with first 1-inch of runoff qu = the unit peak discharge, in csm/in (774 csm/in for Tc associated with 6 minutes) A = impervious surface drainage area (in square miles) = 10,426 sf = 0.000374 square miles WQV = water quality volume in watershed inches

Q = (774 csm/in)\*(0.000374 square miles)\*(1 inch) Q = 0.29 CFS

Required Capacity = 0.29 CFS Ferguson Turret 79% Removal Capacity = 0.50 CFS



#### 0.50 CFS > 0.29 CFS, OK 79% Pretreatment

#### Annual Sediment Volume

Per Town of Groton Stormwater Regulations, all pretreatment devices should be designed to hold an annual sediment loading.

Required Capacity =  $A_s * (500 \text{ lb/Acre-Storm / } 90 \text{ lb/ft}^3) * 10 \text{ storms/year}$ 

 $A_{\rm s}$  = Area to be sanded (acres) = 0.19

Required Capacity = 10.5 ft<sup>3</sup>

Sediment Forebay Capacity = 23 ft<sup>3</sup>

23 ft<sup>3</sup> > 10.5 ft<sup>3</sup> OK



# Standard 4: Stormwater management system to remove 80% of the average annual load of Total Suspended Solids (TSS)

The stormwater management system is designed to remove >80% annual total suspended solids (TSS) from the proposed onsite impervious.

The stormwater management system is designed to remove 80% of the average annual total suspended solids (TSS) from the proposed development.

#### **TSS Removal Calculation**

#### Treatment Train #1: to Porous Pavement

• Porous Pavement: 80% TSS Removal with incorporated treatment course.

100% \* 80% = **80%** 100% - 80% = 20%

#### TSS Removal of the proposed drainage = 80%

Treatment Train #2: Foxhole to Porous Pavement

• Foxhole Pretreatment: 79% (See Flow Based Calcs)

100% \* 79% = 79% 100% - 79% = 21%

• Porous Pavement: 80% TSS Removal with incorporated Pre-Treatment

21% \* 80% = 16.8% 21% - 16.8% = 4.2%

#### TSS Removal of the proposed drainage = 95.8% Treatment Train #3: Overland Flow to Infiltration Basin

• Infiltration: 80%

100% \* 80% = 80% 100% - 80% = 20%

#### TSS Removal of the proposed drainage = 80%

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#### Site-wide Weighted TSS Removal Calculation

• Treatment Train #1

Percentage of Site Impervious = 34,041 sf / 45,408 sf = 75%

Weighted TSS Removal = 80% \* 75% = 60%

• Treatment Train #2

Percentage of Site Impervious = 10,426 sf / 45,408 sf = 23%

Weighted TSS Removal = 95.8% \* 23% = 22%

• Treatment Train #3

Percentage of Site Impervious = 941 sf / 45,408 sf = 2%

Weighted TSS Removal = 80% \* 2% = 1.6%

<u>Total Site-Wide TSS Removal = 60% + 22% + 1.6% = 83.6%</u>



# Standard 5: Land uses with higher potential pollutant loads.

The proposed development is not considered a land use that generally produces higher potential pollutant loads.

# Standard 6: Stormwater discharges to critical areas

This site is not located within or adjacent to a Critical Area.

# Standard 7: Redevelopment projects

The project is not considered a redevelopment project.

# Standard 8: Control construction-related impacts

The project will install erosion and sediment controls prior to any earthwork activity. Erosion control barriers will be placed down slope from the proposed construction and along Forge Village Road to prevent roadway intrusion, to prevent erosion and sedimentation into the surrounding areas. The barriers will be maintained and inspected periodically during construction; sediment buildup will be removed, and any damaged barrier will be replaced as needed. See site plan SWPPP once submitted.

## Standard 9: Long-term operation and maintenance plan

See Appendix A for the operation and maintenance requirements of the stormwater management system.

# Standard 10: No illicit discharges

An illicit discharge compliance statement will be provided by the property owner under separate cover.



# Appendix A: Operation and Maintenance Plan



## **Porous Pavement**

### System Owner: 119 Partners LLC (Or Future Owner)

(Per DEP Stormwater Structural BMP's Vol 2)

In most porous pavement designs, the pavement itself acts as pretreatment to the stone reservoir below. Consequently, frequent cleaning and maintenance of the pavement surface is critical to prevent clogging. To keep the surface clean, frequent vacuum sweeping along with jet washing of asphalt and concrete pavement is required. No winter sanding shall be conducted on the porous surface. As discussed, designs that include an "overflow edge" provide a backup in case the surface clogs. If the surface clogs, stormwater will flow over the surface and into the trench, where some infiltration and treatment will occur. For proper maintenance:

- Post signs identifying porous pavement areas.
- Minimize salt use during winter months. If drinking water sources are located nearby (see setbacks), porous pavements may not be allowed.
- No winter sanding is allowed.
- Keep landscaped areas well maintained to prevent soil from being transported onto the pavement.
- Clean the surface using vacuum sweeping machines monthly. For paving stones, periodically add joint material (sand) to replace material that has been transported.
- Regularly monitor the paving surface to make sure it drains properly after storms.
- Never reseal or repave with impermeable materials.
- Inspect the surface annually for deterioration or spalling.
- Periodically reseed grass pavers to fill in bare spots.
- Attach rollers to the bottoms of snowplows to prevent them from catching on the edges of grass pavers and some paving stones.

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Date	Inspector	Condition	Maintenance Performed*

\*Evidence of maintenance (i.e. receipts) must be provided.



# Ferguson Rain Guardian Foxhole

#### System Owner: 119 Partners LLC (Or Future Owner) (Per DEP Stormwater Structural BMP's Vol 2)

Depending on the characteristics of the contributing watershed and seasonal variation, common maintenance needs include periodic removal of accumulated leaves (and other organic debris) and garbage from the top grate and sediment and fine debris from the concrete dry filter box. The Rain Guardian will have surface trash removed monthly via handpicking and shall be cleaned at least four times per year. More frequent cleanings may be needed, and the unit shall be checked for debris, clogging, and sediment levels after each rain event.

If sediment accumulates beyond an acceptable level in the system, it will be necessary to remove. This can be done by manual removal with a shovel or mechanical device. The filter screen can be cleaned manually through brushing or with pressurized water.

Date	Inspector	Condition	Maintenance Performed*

\*Evidence of maintenance (i.e. receipts) must be provided

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# Yard Drains

#### System Owner: 119 Partners LLC (Or Future Owner) (Per DEP Stormwater Structural BMP's Vol 2)

See Manufacturer Specification\*

Date	Inspector	Condition	Maintenance Performed*

\*Evidence of maintenance (i.e. receipts) must be provided



## Sediment Forebay

#### System Owner: 119 Partners, LLC (Or Future Owner) (Per DEP Stormwater Structural BMP's Vol 2)

In many cases, a landscaping contractor working elsewhere on the site can complete maintenance tasks. Stabilize the floor and sidewalls of the sediment forebay before making it operational, otherwise the practice will discharge excess amounts of suspended sediments.

Inspect and clean out the sediment forebay to assure that sediments and associated pollutants are cleaned out. Frequently removing accumulated sediments will make it less likely that sediments will be resuspended. At a minimum, inspect the sediment forebays monthly and clean them out at least four times a year.

Mow the grass areas and keep the grass height no greater than 6 inches. Check for signs of rilling and gullying and repair as needed. After removing the sediment, replace any vegetation damaged during the clean-out by either reseeding or resodding. When reseeding, incorporate practices such as hydroseeding with a tackifier, blanket, or similar practice to ensure that no scour occurs in the forebay, while the seeds germinate and develop roots.

Date	Inspector	Condition	Maintenance Performed*

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# Infiltration Basin

### System Owner: Dunstable Ledge, LLC

(Per DEP Stormwater Structural BMP's Vol 2)

In many cases, a landscaping contractor working elsewhere on the site can complete maintenance tasks. Inspect the basin and outlet structure to ensure no structural damage has occurred and that they are functioning properly and up to design standards.

Inspection and preventive maintenance is required at least twice per year, and after each major storm event. Note how long water remains standing in the basin after a storm. If water remains standing after 48 to 72 hours after a storm, the infiltration basin may be clogged.

At least twice per year, mow the buffer area, side slopes, and basin bottom. Remove grass clippings, accumulated organic matter, trash and debris at this time.

Remove sediment from the basin as necessary when the basin is dry. Use light equipment when removing the top layer, as to not compact the underlying soil. Use deep tilling to break and remove any clogged surfaces and revegetate immediately.

Important items to check during inspections include:

- Signs of differential settlement
- Cracking
- Erosion
- Leakage in the embankments
- Tree growth on the embankments
- Condition of rip rap
- Sediment accumulation
- Health of vegetation, turf

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Date	Inspector	Condition	Maintenance Performed*

\*Evidence of maintenance (i.e. receipts) must be provided



## Riprap at Flared End Sections

System Owner: 119 Partners, LLC (Or Future Owner)

Riprap is pertinent to the protection of slopes and other areas subject to erosion by the flow of stormwater. Proper maintenance helps to reduce the impact of erosion and ensure the longevity of slope stability.

Riprap shall be checked at least annually and after every major storm event for displaced stones, slumping, and erosion at edges, especially downstream or downslope. If riprap has been damaged, it should be repaired immediately before further damage occurs.

Woody vegetation should be removed from the rock riprap annually. Tree roots and other debris can aid in dislodging riprap and causing erosion.

Date	Inspector	Condition	Maintenance Performed*



# **Appendix B: Erosion and Sediment Control Notes and Construction General Sequence**



# **Erosion and Sediment Control Notes**

- A. Erosion and sediment control measures must be installed prior to the start of construction and maintained and upgraded as necessary during construction by the contractor. It is the contractor's responsibility to inspect and install additional control measures as needed during construction.
- B. All catch basins receiving drainage from the project site must be provided with a catch basin filter.
- C. Stabilization of all re-graded and soil stockpile areas must be maintained during all phases of construction.
- D. Sediment removed from erosion and sediment control devices must be properly removed and disposed. All damaged erosion controls must be removed and replaced.
- E. The contractor is responsible for implementing the erosion and sediment control plan. This includes the installation and maintenance of control measures, informing all parties engaged on the construction site of the requirements and objectives of the plan, and notifying the proper city agency of any transfer of this responsibility.
- F. The contractor shall be responsible for controlling wind erosion and dust throughout the life of his contract. Dust control may include, but is not limited to, sprinkling of water on exposed soils and street sweeping adjacent roadways.
- G. If final grading is to be delayed for more than 21 days after land disturbance activities cease, temporary vegetation or mulch shall be used to stabilize soils within 14 days of the last disturbance.
- H. If a disturbed area will be exposed for greater than one year, permanent grasses or other approved cover must be installed.
- I. The contractor must keep on-site at all times additional silt fence and hay bales for the installation at the direction of the engineer or the city to mitigate any emergency condition.
- J. The construction fencing and erosion and sediment controls as shown may not be practical during all stages of construction. Earthwork activity on-site must be done in a manner such that runoff is directed to a sediment control device or infiltrated to the ground.
- K. Demolition and construction debris must be properly contained and disposed of.
- L. Disposal of all demolished materials is the responsibility of the contractor and must be hauled off-site in accordance with all federal, state and local requirements.

# General Construction Sequence

- 1. Install erosion and sediment controls prior to starting any earthworks activity.
- 2. Begin clearing, grubbing and demolition.
- 3. Begin road grading and utility installations.
- 4. Construct building foundation.
- 5. Install site furnishings.
- 6. Install landscaping.
- 7. Erosion and sediment controls shall be maintained until permanent cover is established.





# **Appendix C: Rain Guardian Foxhole**





# RAIN GUARDIAN TURRET AND FOXHOLE ENGINEERING PROPERTIES

## **RAIN GUARDIAN TURRET:**

### Turret Flow Rate Capacity:

Outflow is possible through three locations. Please note the vertical filter within the chamber was assumed to be 100% clogged because its primary function is to allow the chamber to dry out between rain events.

1) Filter overflow – water can pass between the top of the filter and the bottom of the metal grate; calculated using the continuity equation (i.e.  $Q=V^*A$ )

2) Grate overflow – water can pass through the top metal grate beyond the vertical filter wall; calculated using an orifice equation (i.e.  $Q=0.0108*A*\sqrt{d}$ )

3) High volume overflow – water can overtop the front debris wall onto the splash pad; calculated using a standard broad crested weir equation (i.e.  $Q=C*L*H^{(3/2)}$ )

Filter overflow – 0.45 CFS

Grate overflow – 2.59 CFS

Emergency overflow - 0.41 CFS

**TOTAL: 3.45 CFS** 

Turret Internal Storage Vol: (i.e. storage capacity below the top of the filter wall): 4.02 ft<sup>3</sup>

### **RAIN GUARDIAN FOXHOLE:**

Below are the flow and storage data for the Rain Guardian Foxhole with an inlet, middle, and outlet (i.e. 6' top lid). (the addition of mid section (for longer units) would improve the sediment storage capacity).

### Foxhole Flow Rate Capacity:

Outflow is possible through three locations. Please note the vertical filter within the chamber was assumed to be 100% clogged because its primary function is to allow the chamber to dry out between rain events.

1) Filter overflow – water can pass between the top of the filter and the bottom of the metal grate; calculated using the continuity equation (i.e.  $Q=V^*A$ )

2) Grate overflow – water can pass through the top metal grate beyond the vertical filter wall; calculated using an orifice equation (i.e.  $Q=0.0108*A*\sqrt{d}$ )

3) High volume overflow – water can overtop the front debris wall onto the splash pad; calculated using a standard broad crested weir equation (i.e.  $Q=C*L*H^{(3/2)}$ )

Filter overflow – 0.30 CFS Grate overflow – 2.69 CFS Emergency overflow - 0.52 CFS TOTAL: **3.51 CFS** 

<u>Foxhole Internal Storage Volume</u> (i.e. storage capacity below the top of the filter wall):

Inlet + Outlet:  $2.0 \text{ ft}^3$ 

Middle:  $2.65 \text{ ft}^3$ 

TOTAL: 4.65 ft<sup>3</sup>

# MODULAR CONCRETE DRY FILTER BOX DROP-IN SPECIFICATION

November 2022

The following specification is a sample guideline to be customized by the engineer as needed for preparing a site-specific specification. This information is provided for reference purposes only and is not intended as a warranty or guarantee.

#### **DROP-IN SPECIFICATION**

#### MODULAR CONCRETE DRY FILTER BOX FOR SURFACE BMPS

- 1. AUTHORIZED PRODUCTS
  - 1.1. The modular concrete dry filter box shall be a Rain Guardian Foxhole Pretreatment Chamber (U.S. Patent Nos. 8,501,016 and 8,858,804).
- 2. AUTHORIZED SUPPLIERS
  - 2.1. Minnesota, Alaska, and Hawaii
    - 2.1.1. Anoka Conservation District 1318 McKay Dr. NE, Suite 300 Ham Lake, MN 55304 (763) 434-2030 ext. 15 AnokaSWCD.org | RainGuardian.biz
  - 2.2. Wisconsin
    - 2.2.1. Anoka Conservation District 1318 McKay Dr. NE, Suite 300 Ham Lake, MN 55304 (763) 434-2030 ext. 15 AnokaSWCD.org | RainGuardian.biz
    - 2.2.2. Ferguson Enterprises, LLC doing business as Ferguson Waterworks 12500 Jefferson Avenue Newport News, VA 23602
  - 2.3. Alabama, Arizona, Arkansas, California, Colorado, Connecticut, Delaware, Florida, Georgia, Idaho, Illinois, Indiana, Iowa, Kansas, Kentucky, Louisiana, Maine, Maryland, Massachusetts, Michigan, Mississippi, Missouri, Montana, Nebraska, Nevada, New Hampshire, New Jersey, New Mexico, New York, North Carolina, North Dakota, Ohio, Oklahoma, Oregon, Pennsylvania, Rhode Island, South Carolina, South Dakota, Tennessee, Texas, Utah, Vermont, Virginia, Washington, West Virginia, and Wyoming
    - 2.3.1. Ferguson Enterprises, LLC doing business as Ferguson Waterworks 12500 Jefferson Avenue Newport News, VA 23602
- 3. AUTHORIZED MANUFACTURERS
  - 3.1. Stoneworks Architectural Precast/Cast Stone

11555 205<sup>th</sup> Ave. NW Elk River, MN 55330 (763) 633-2200 stoneworksap.com

- 4. INTRODUCTION
  - 4.1. Scope
    - 4.1.1. This specification details requirements for proper design, installation, and maintenance of a modular concrete dry filter box for surface stormwater best management practices (BMP).

- 4.2. Product Summary
  - 4.2.1. A modular concrete dry filter box is a pretreatment structure installed at grade with a curb-cut or curb inlet opening that allows water to enter a high performance modular biofiltration system, bioretention, rain garden, bioswale, or similar stormwater BMP.
  - 4.2.2. The modularity of the box (i.e. inlet, middle, and outlet sections) allows for variable box lengths to span desired distances.
  - 4.2.3. The box includes a removable, load-bearing lid that allows nearby surface elevations (e.g. sidewalk, trail, or boulevard) to be maintained.
  - 4.2.4. The box provides a stable inlet, reduces runoff velocities, and captures gross pollutants; therefore, simplifying the recurring sediment removal and surface erosion common with turf, rip rap, or smooth concrete inlet aprons.
  - 4.2.5. Capturing sediment within the box helps extend the life of a downstream primary treatment BMP by reducing the sediment load and internal scour/erosion.
  - 4.2.6. Modular concrete dry filter boxes can be installed on both new and existing projects where there are concerns about inlet stability and/or maintenance issues.

### 5. SPECIFICATIONS

- 5.1. Functional components of the modular concrete dry filter box must include the components listed below and meet the standards in Table 1.
  - 5.1.1. Top grate
    - 5.1.1.1. Top grate mechanically separates larger debris pieces (e.g. leaf litter and garbage) from stormwater runoff, thereby increasing storage space for sediment and finer debris within the unit. In addition, the top grate of the box must minimally support pedestrian foot traffic loads for maintenance purposes.
  - 5.1.2. Impermeable side walls
    - 5.1.2.1. Impermeable side walls which, when connected to a water permeable filter sidewall, create a debris and sediment trap. Chamber therefore allows heavier solids to settle and collect in an easy to clean location. The side walls also contain flow, thereby preventing inlet erosion.
  - 5.1.3. Water permeable filter sidewall
    - 5.1.3.1. The water permeable filter sidewall is independently connected to the impermeable side walls. The permeable filter allows for the box to dry out between runoff events, easing maintenance by preventing the need to remove sediment/debris in a slurry state. It also prevents anoxic conditions and habitat for mosquito reproduction.
  - 5.1.4. Impermeable debris walls
    - 5.1.4.1. Impermeable debris walls capture floatables when BMP is filled to capacity (e.g. leaf litter and seeds) and prevent transfer of floatables between the inlet and BMP.
  - 5.1.5. High volume overflow points

- 5.1.5.1. The modular concrete dry filter box must provide for high volume overflow during large storm events such that water within the structure does not overtop the sidewalls, which would reduce the box's ability to retain floatables and maintain a stable inlet. The overflow points also ensure stormwater will not bypass the BMP until it reaches capacity.
- 5.1.6. Splash pad
  - 5.1.6.1. The box should include a splash pad downstream of the principal (permeable filter wall) and emergency overflow (concrete weir) points to reduce scouring below the box (i.e. within the aggregate base and BMP soil).
- 5.1.7. Top lid
  - 5.1.7.1. Each inlet/outlet combination and each middle section shall have a fiber reinforced plastic (FRP) composite lid with concentrated load capacity of 11,200 lbs.
- 5.1.8. All components must be easy to clean without specialized equipment.

Table 1: Modular concrete dry filter box standards.

MODULAR SECTION	PROPERTY OF STRUCTURE(S)	VALUE OR METHOD
Inlet, Middle, and Outlet	Steel reinforced, cold joint secured monolithic concrete structure, weight and standard exterior dimensions	INLET - 875 lbs. 2'-8.25"L x 2'-11"W x 1'-7"H MIDDLE - 965 lbs. 3'-0.5"L x 2'-11"W x 1'-7"H
		OUTLET - 730 lbs. 2'-6"L x 2'-11"W x 1'-7"H
Inlet, Middle, and Outlet	Concrete minimum compressive strength	4,500 psi at 28 days
Inlet, Middle, and Outlet	Concrete air entrained	5-8.5% by volume
Inlet, Middle, and Outlet	Manufactured and designed standard	ASTM C858

### 6. DELIVERY, STORAGE, AND HANDLING

- 6.1. Delivery
  - 6.1.1. Delivery of a modular concrete dry filter box must be from an authorized supplier.
  - 6.1.2. Reasonable accommodations should be made to protect all materials from damage during delivery. Shipments should be inspected upon arrival to insure no damage occurred during transportation. Any damage found after delivery will be the responsibility of the contractor.
- 6.2. Storage and Handling
  - 6.2.1. Storage prior to installation should occur on smooth surfaces, free from dirt, mud, and debris. Boxes are designed to persist in all seasons so temperature and precipitation should not be a problem.

### 7. INSTALLATION

- 7.1. A modular concrete dry filter box should rest on a level, solid base to prevent settling. A well-draining aggregate base material (minimum 6" thickness) should be compacted to 95% percent standard proctor. The aggregate base should have a surface area equal to or larger than the modular concrete dry filter box base.
- 7.2. The aggregate base location and distance behind the curb depends on site considerations but considerations should include bioretention basin side slopes and inlet slope to promote water flow into the unit.
- 7.3. The monolithic box sections (i.e. inlet, middle, and outlet) include a 4" concrete base to provide a foundation for the chamber structure and to supply a splash pad for water entering the unit.
- 7.4. Excavation at the unit installation location should ensure sufficient depth for the 6" aggregate base, modular concrete dry filter box base, and ponding depth of the bioretention practice. For example, if the ponding depth of the basin is

designed to be 9" and the modular concrete dry filter box base is 4", then soil should be excavated to 1'-7" (9" ponding depth, 6" aggregate base, 4" filter box base).

- 7.5. Set inlet first, followed by middle section(s), and finally the outlet on the prepared aggregate base. Position outlet piece so primary outlet aligns with toe of basin side slope to avoid soil interference with removable filter wall.
- 7.6. Secure modular pieces at each joint using provided galvanized tie rods.
- 7.7. Install water permeable filter, top grate(s), and top lid(s).
- 7.8. Stormwater is most commonly directed into the box via a curb-cut or concrete inlet. Said inlet should be framed from the back of the curb to the unit inlet prior to pouring. Top elevations of the framing should match the top of the curb on the street side and the top of the filter box at the inlet to the box. Expansion joint material should be used between the concrete curb and modular concrete dry filter box.
- 7.9. Side curbs of the poured inlet must have an insurmountable profile to prevent water flow from overtopping the downstream side of the inlet.
- 7.10. The slope of the inlet from the gutter to the filter box must be large enough to promote the inflow of water to the filter box.

#### 8. OPERATION

- 8.1. Items below assume proper installation of the modular concrete dry filter box based on design guidelines.
  - 8.1.1. Stormwater entering the box via a curb-cut or concrete inlet must pass through the top grate. The grate provides for mechanical sorting of larger debris such as leaves and garbage.
  - 8.1.2. Once in the box, the vertical, permeable filter wall allows for settling within the box and filtration of stormwater through the permeable filter screen. Should the filter screen clog or the unit fill, maintenance will be required.
  - 8.1.3. As the box and BMP fill, the water level rises and the top debris walls of the box restrict floatable debris from entering or exiting the BMP.
  - 8.1.4. Cold climate suitability
    - 8.1.4.1. During winter, modular concrete dry filter boxes will likely become buried in snow and ice which is no different from any other inlet type. Runoff will likely continue to enter the box beneath the snow or when an open pathway is formed during snowmelt. When properly designed and installed, modular concrete dry filter boxes will not shift or separate from the inlet as the ground freezes and thaws.

#### 9. MAINTENANCE

9.1. Depending on the characteristics of the contributing watershed and seasonal variation, common maintenance needs include periodic removal of accumulated leaves (and other organic debris) and garbage from the top grate and sediment and fine debris from the modular concrete dry filter box. Contributing watersheds with high sediment concentrations may require up to monthly or twice monthly visits to satisfy maintenance needs.

9.2. If sediment accumulates beyond an acceptable level in the system, it will be necessary to remove. This can be done by manual removal with a shovel or vacuum device. The filter screen can be cleaned manually through brushing or with pressurized water.

### 10. PAYMENT

- 10.1. Payment of modular concrete dry filter boxes shall be based on a per unit price and may or may not include delivery of the box to the project site. The contractor is responsible for determining the style/configuration of box needed.
- 10.2. Total cost will be provided by the distributor based on unit costs requested delivery fees, handling fees, and associated taxes.

# RAIN GUARDIAN™ FOXHOLE TYPICAL DETAIL



#### **SPECIFICATIONS**

1. STEEL REINFORCED, COLD JOINT SECURED MONOLITHIC CONCRETE STRUCTURES (INLET 875 LBS, MIDDLE 965 LBS, AND OUTLET 730 LBS). CONCRETE SHALL HAVE A MINIMUM COMPRESSIVE STRENGTH OF 4,500 PSI AT 28 DAYS. CONCRETE AIR ENTRAINED (5% TO 8.5% BY VOLUME). MANUFACTURED AND DESIGNED TO ASTM C858. 2. 2-POINT PICK USING RECESSED LIFTING POCKETS WITH A STANDARD HOOK.

3. FIBERGLASS GRATE (11 LBS/PIECE).

4. FRP COMPOSITE LID (38 LBS/PIECE) WITH CONCENTRATED LOAD CAPACITY OF 11,200 LBS.

#### **INSTALLATION NOTES**

1. INSTALL A CLASS 5 BASE (COMPACTED TO 95% STANDARD PROCTOR). IT IS CRITICAL THAT THE CLASS 5 BASE IS EVEN TO ENSURE THE FOXHOLE PIECES ALIGN VERTICALLY SUCH THAT THE TOP LIDS LAY FLUSH WITH THE TOP OF THE FOXHOLE PIECES AND ADJACENT BOULEVARD, SIDEWALK, OR PATH. THE DISTANCE FROM THE BACK OF THE CURB MAY VARY BASED ON SITE CONDITIONS. EXCAVATE 1' 7" BELOW THE GUTTERLINE ELEVATION (I.E. THE BIORETENTION OVERFLOW ELEVATION) TO ACCOMMODATE THE 9" PONDING DEPTH, 6" CLASS 5 AGGREGATE, AND 4" RAIN GUARDIAN FOXHOLE BASE (INCLUDED). THEREFORE, THE TOP OF THE CLASS 5 COMPACTED BASE IS PRECISELY 1' 1" BELOW THE GUTTERLINE ELEVATION. THE TOP OF THE RAIN GUARDIAN FOXHOLE INLET POINT WILL BE 7-1/2" ABOVE THE TOP OF THE CONCRETE BASE AND 1-1/2" BELOW THE GUTTERLINE ELEVATION TO ACCOMMODATE A SLOPED INLET FROM THE GUTTER TO THE RAIN GUARDIAN FOXHOLE.

2. SET RAIN GUARDIAN FOXHOLE INLET FIRST, FOLLOWED BY MIDDLE SECTION(S), AND FINALLY THE OUTLET ON THE PREPARED CLASS 5 BASE. POSITION RAIN GUARDIAN FOXHOLE OUTLET PIECE SO PRIMARY OUTLET ALIGNS WITH TOE OF BASIN SIDE SLOPE TO AVOID SOIL INTERFERENCE WITH REMOVABLE FILTER WALL.

3. SECURE MODULAR FOXHOLE PIECES AT EACH JOINT USING PROVIDED GALVANIZED TIE RODS.

4. INSTALL EXPANSION/CONTRACTION JOINT MATERIAL OR A SHEET OF POLY TO SERVE AS A BOND BREAK BETWEEN RAIN GUARDIAN FOXHOLE AND CONCRETE INLET BEFORE POURING INLET.

5. REMOVABLE FILTER WALL SHOULD BE INSTALLED WITH FILTER FABRIC FACING THE RAIN GUARDIAN FOXHOLE INLET.

#### **REVISION HISTORY**

REV	BY	DATE	DESCRIPTION	
А	MDH	11/16/2022	MODULAR FOXHOLE	
SCALE		VARIABLE		
U.S. PATENT NOS.		8,501,016 AND 8,858,804		





# RAIN GUARDIAN<sup>TM</sup> INSTALLATION



1318 MCKAY DR. NE, SUITE 300 HAM LAKE, MN 55304 (763) 434-2030 (M-F 8:00-4:30) WWW.ANOKASWCD.ORG

### **OVERVIEW**



SLAB DIMENSIONS, DISTANCE FROM CURB, AND CHAMBER ELEVATION VARIES WITH SITE CONDITIONS. THE TOP OF THE METAL GRATE, HOWEVER, SHOULD BE 1.5" - 2" BELOW THE GUTTER AND THE CONCRETE SLAB SHOULD EXTEND WELL BEYOND THE FILTER WALL TO SERVE AS A SPLASH DISSIPATER.

### CONCRETE BASE



EXCAVATE 16" BELOW THE DOWNSTREAM GUTTER ELEVATION (I.E. THE RAIN GARDEN OVERFLOW ELEVATION) TO ACCOMMODATE THE 4" CONCRETE BASE. THEREFORE, THE TOP OF THE CONCRETE BASE IS 12" BELOW THE RAIN GARDEN OVERFLOW ELEVATION.

The concrete base is set 22" from the back of the existing curb and centered on the proposed curb-cut. The concrete is then poured into a wooden frame with interior dimensions of 54"L x 30"W x 4"H.





REBAR IS PLACED DIAGONALLY AFTER 2" OF CONCRETE HAVE BEEN POURED TO PROVIDE REINFORCEMENT OF THE CON-CRETE BASE.
#### **RAIN GUARDIAN PLACEMENT AND SECURING**



RAIN GUARDIAN PLACEMENT IS SET 26" FROM THE BACK OF THE EXISTING CURB. ENSURE THE CONCRETE BASE EXTENDS AT LEAST 4" BEYOND THE FILTER WALL TO SERVE AS A SPLASH DISSI-PATER. APPLY ADHESIVE TO BASE OF RAIN GUARDIAN AND POSITION ON CONCRETE BASE. USE ADDITIONAL ADHESIVE AROUND BASE OF INTERIOR TO ESTABLISH WATER-TIGHT SEAL. USING PI-LOT HOLES IN CORNER POSTS, DRILL 3/16" HOLES INTO CONCRETE WITH 6 1/2" MASONRY BIT AND HAMMER DRILL. SECURE WITH 1/4" x 5" MASONRY SCREWS (PROVIDED).

#### CURB-CUT AND APRON



When Pouring the concrete inlet, ensure the carriage bolts on the Rain Guardian are surrounded by at least 2" of concrete on all sides. The top of the Rain Guardian grate will be 10.5" above the top of the concrete base and 1.5" below the rain garden overflow elevation to accommodate a sloped apron from the gutter to the Rain Guardian.



FILL VOID BETWEEN EXISTING CURB AND RAIN GUARDIAN. IN-STALL FRAMING TO PREPARE FOR CURB-CUT AND APRON IN-STALLATION. SIDES OF APRON SHOULD BE RAISED SIGNIFI-CANTLY TO BLEND INTO CURB AND MATCH TOP HEIGHT OF RAIN GUARDIAN SIDE DEBRIS WALL.



#### MAINTENANCE



SEDIMENT, LEAVES, AND GRASS CLIPPINGS TRAPPED INSIDE THE CHAMBER ARE EASILY REMOVED BY THE LANDOWNER WITH A SHOVEL. THE DROP-IN FILTER WALL CAN BE EITHER SWEPT CLEAN OR RINSED WITH A GARDEN HOSE TO MAINTAIN OPTIMAL FIL-TRATION CAPACITY.





# **Appendix D: Pre and Post Drainage Maps**



2024 L:\17267\CURRENT\17267 Drainage.dwg

N/F KEVIN G. & LYNN R. PAMMETT BK/PG 27977/494 YR/PL 1978/492 (LOT 1) 33 FORGE VILLAGE RD MAP-PID 133-13-0	<b>DEF</b> <b>EXAMPLE FOR</b> <b>EXAMPLE FOR</b>
S LLC /597 /043 RD 49=0 49=0 K-KE KON POST 14"PIN 0 16"PIN 0 18"PIN 24"PIN 24"PIN 0 0 0 0 0 0 0 0 0 0 0 0 0	PROPOSED AGE RESTRICTED HOUSING DEVELOPMENT 797 BOSTON ROAD GROTON, MA 01450
N/F STEPHEN L. & BARBARA J. SMITH BK/PG 13203/151 YR/PL 1959/1851 (LOT 4) 26 FORGE VILLAGE RD MAP-PID 133-48-0 R APPROX. PL. P P P P P P P P P P P P P	REVISIONS:           NO         BY         DATE         DESCRIPTION           1         KF         04/17/24         REV. PER PEER REVIEW           -         -         -         -           -         -         -         -           -         -         -         -           -         -         -         -           -         -         -         -           -         -         -         -           -         -         -         -           -         -         -         -           -         -         -         -           -         -         -         -           -         -         -         -           -         -         -         -           -         -         -         -           -         -         -         -           -         -         -         -           -         -         -         -           -         -         -         -           -         -         -         -           -         -
(LOT 5) 12 DOROTHY PLACE MAP-PID 133-47-0 R APPROX. PL. R R - R - R	DRAINAGE PLAN PRE-CONDITION DRAINAGE PLAN DATE: 2/16/2024 REQUECT NUMBER: 17267
20 0 20 40 SCALE IN FEET	DESIGNED BY: NC DRAWN BY: NC CHECKED BY: KE 1 SHEET 1 OF 2

![](_page_39_Figure_0.jpeg)

![](_page_40_Picture_0.jpeg)

# **Appendix E: Cut/Fill Analysis**

CutFillReport.html

# **Cut/Fill Report**

Generated:	2024-04-17 14:14:13
By user:	nclegg
Drawing:	L:\17267\CURRENT\L:\17267\CURRENT\17267 Cut Fill.dwg

Volume Summary										
Name	Туре	Cut Factor	Fill Factor	<b>2d Area</b> (Sq. Ft.)	<b>Cut</b> (Cu. Yd.)	<b>Fill</b> (Cu. Yd.)	Net (Cu. Yd.)			
Cut Fill Analysis	full	1.000	1.000	88845.36	386.11	2004.32	1618.21 <fill></fill>			

Totals				
	<b>2d Area</b> (Sq. Ft.)	<b>Cut</b> (Cu. Yd.)	<b>Fill</b> (Cu. Yd.)	Net (Cu. Yd.)
Total	88845.36	386.11	2004.32	1618.21 <fill></fill>

\* Value adjusted by cut or fill factor other than 1.0

![](_page_42_Picture_0.jpeg)

## **Appendix F: HydroCAD Report**

![](_page_43_Figure_0.jpeg)

#### **Project Notes**

Rainfall events imported from "NRCS-Rain.txt" for 4253 MA Rowley Essex County Rainfall events imported from "NRCS-Rain.txt" for 4114 MA Groton Middlesex County North Rainfall events imported from "Groton 40B Post Drainage.hcp" Rainfall events imported from "Groton 40B Post Drainage.hcp"

Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
1	2-Year	Type III 24-hr		Default	24.00	1	3.15	2
2	10-Year	Type III 24-hr		Default	24.00	1	4.86	2
3	25-Year	Type III 24-hr		Default	24.00	1	5.92	2
4	100-Year	Type III 24-hr		Default	24.00	1	7.56	2

#### **Rainfall Events Listing**

#### Area Listing (all nodes)

Area	n CN	Description
(sq-ft)	)	(subcatchment-numbers)
6,365	5 72	Dirt roads, HSG A (S101)
98,934	68	Open space, such as lawns, parks, and cemeteries, HSG A (S101)
5,875	5 98	Paved parking, HSG A (S101)
16,689	30	Woods and forest, HSG A (S101)
127,863	65	TOTAL AREA

#### Soil Listing (all nodes)

Area	Soil	Subcatchment
(sq-ft)	Group	Numbers
127,863	HSG A	S101
0	HSG B	
0	HSG C	
0	HSG D	
0	Other	
127,863		TOTAL AREA

## Groton 40B Pre Drainage

Prepared by Howard Stein H	ludson Associates
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Printed 4/17/2024 Page 6

HSG-A (sq-ft)	HSG-B (sq-ft)	HSG-C (sq-ft)	HSG-D (sq-ft)	Other (sq-ft)	Total (sq-ft)	Ground Cover
6,365	0	0	0	0	6,365	Dirt roads
98,934	0	0	0	0	98,934	Open space, such as lawns, parks, and cemeteries
5,875	0	0	0	0	5,875	Paved parking
16,689	0	0	0	0	16,689	Woods and forest
127,863	0	0	0	0	127,863	TOTAL AREA

#### Ground Covers (all nodes)

# Line# Node Number Notes 1 Project Rainfall events imported from "NRCS-Rain.txt" for 4253 MA Rowley Essex County 2 Rainfall events imported from "NRCS-Rain.txt" for 4114 MA Groton Middlesex County North 3 Rainfall events imported from "Groton 40B Post Drainage.hcp" 4 Rainfall events imported from "Groton 40B Post Drainage.hcp"

#### Notes Listing (all nodes)

<b>Groton 40B Pre Drainage</b> Prepared by Howard Stein Hudson Ass	Type III 24-hr	2-Year Rainfall=3.15" Printed 4/17/2024	
HydroCAD® 10.20-4a s/n 02930 © 2023 Hy	droCAD Software Solutions	LLC	Page 8
Time span=0.	00-24.00 hrs, dt=0.05 hrs,	481 points	nd method
Runoff by SCS T	R-20 method, UH=SCS,	Weighted-CN	
Reach routing by Dyn-Stor-I	nd method - Pond routin	g by Dyn-Stor-Ir	
Subcatchment S101: S101	Runoff Area=127,863 s	f 4.59% Impervi	ous Runoff Depth>0.57"
	Flow Length=427' Tc=24	.9 min CN=65	Runoff=0.95 cfs 6,090 cf

Pond 1P: Ex Site DepressionPeak Elev=261.37'Storage=2,130 cfInflow=0.95 cfs6,090 cfDiscarded=0.18 cfs5,656 cfPrimary=0.00 cfs0 cfOutflow=0.18 cfs5,656 cf

Link AP1: Abutters

Inflow=0.00 cfs 0 cf Primary=0.00 cfs 0 cf

Total Runoff Area = 127,863 sf Runoff Volume = 6,090 cf Average Runoff Depth = 0.57"95.41% Pervious = 121,988 sf4.59% Impervious = 5,875 sf

#### Summary for Subcatchment S101: S101

Runoff = 0.95 cfs @ 12.44 hrs, Volume= Routed to Pond 1P : Ex Site Depression 6,090 cf, Depth> 0.57"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.15"

	A	rea (sf)	CN D	escription		
*		98,934	68 C	)pen space	e, such as l	awns, parks, and cemeteries, HSG A
*		16,689	30 V	Voods and	forest, HS	G A
		5,875	98 F	aved park	ing, HSG A	ч.
		6,365	72 E	)irt roads, I	HSG A	
	1	27,863	65 V	Veighted A	verage	
	1	21,988	9	5.41% Per	vious Area	
		5,875	4	.59% Impe	ervious Area	а
	Та	Longth	Clana	Valaaitu	Consoitu	Description
	(min)	(foot)	Siope (ff/ff)			Description
	15.0	(IEEL) 50			(015)	Shoot Flow
	15.0	50	0.0110	0.05		Woods: Light underbrush n= 0.400 P2= 3.15"
	02	6	0 0110	0 52		Shallow Concentrated Flow
	0.2	Ū	0.0110	0.02		Woodland $Kv = 5.0 \text{ fps}$
	0.8	37	0.0110	0.73		Shallow Concentrated Flow.
						Short Grass Pasture Kv= 7.0 fps
	0.9	54	0.0200	0.99		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	0.1	12	0.0200	2.28		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
	6.3	187	0.0050	0.49		Shallow Concentrated Flow,
		~~~				Short Grass Pasture Kv= 7.0 fps
	0.5	38	0.0300	1.21		Shallow Concentrated Flow,
	0.2	40	0 4000	0.04		Short Grass Pasture KV= 7.0 fps
	0.3	43	0.1000	2.21		Sharlow Concentrated Flow,
						Short Grass Pasture KV- 1.0 lps

24.9 427 Total

#### Summary for Pond 1P: Ex Site Depression

Inflow Area	a =	127,863 sf,	4.59% In	npervious,	Inflow Depth >	0.57"	for 2-Ye	ear event
Inflow	=	0.95 cfs @	12.44 hrs,	Volume=	6,090 c	f		
Outflow	=	0.18 cfs @	14.27 hrs,	Volume=	5,656 c	f, Atten	= 81%,	Lag= 110.1 mi
Discarded	=	0.18 cfs @	14.27 hrs,	Volume=	5,656 c	f		•
Primary	=	0.00 cfs @	0.00 hrs,	Volume=	0 c	f		
Routed	to Link A	AP1 : Abutter	S					

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 261.37' @ 14.27 hrs Surf.Area= 3,306 sf Storage= 2,130 cf

Plug-Flow detention time= 162.0 min calculated for 5,656 cf (93% of inflow) Center-of-Mass det. time= 127.6 min (1,037.6 - 910.0)

#### Groton 40B Pre Drainage

Type III 24-hr 2-Year Rainfall=3.15" Printed 4/17/2024 LLC Page 10

Prepared by	y Howar	d Stein H	udson As	sociates	S	
HydroCAD®	, 10.20-4a	s/n 02930	© 2023 H	ydroCAD	Software S	Solutions LL

Volume	Invert	Avail.Sto	rage Storage	e Description			
#1	260.00'	5,42	22 cf Custon	n Stage Data (Pri	ismatic) Listed	l below (Recalc)	
Elevatior (feet	n Su	rf.Area (sɑ-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)			
260.00 261.00 262.00 262.10	) ) ) )	215 2,056 5,425 5,500	0 1,136 3,741 546	0 1,136 4,876 5,422			
Device	Routing	Invert	Outlet Devic	es			
#1 #2	Discarded Primary	260.00' 262.00'	2.410 in/hr E 120.0' long Head (feet) Coef. (Englis	<b>xfiltration over S</b> <b>x 20.0' breadth E</b> 0.20 0.40 0.60 sh) 2.68 2.70 2.	Surface area Broad-Crested 0.80 1.00 1.2 70 2.64 2.63	Phase-In= 0.01' <b>Rectangular Weir</b> 0 1.40 1.60 2.64 2.64 2.63	

**Discarded OutFlow** Max=0.18 cfs @ 14.27 hrs HW=261.37' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.18 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=260.00' TW=0.00' (Dynamic Tailwater) ←2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

#### **Summary for Link AP1: Abutters**

Inflow A	rea =	127,863 sf,	4.59% Impervious,	Inflow Depth = 0.00"	for 2-Year event
Inflow	=	0.00 cfs @	0.00 hrs, Volume=	0 cf	
Primary		0.00 cfs @	0.00 hrs, Volume=	0 cf, Atter	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Groton 40B Pre Drainage		Туре	III 24-hr	10-Year Rainfa	all=4.86"
Prepared by Howard Stein Hudson A	ssociates			Printed 4	/17/2024
HydroCAD® 10.20-4a s/n 02930 © 2023 H	lydroCAD Software S	olutions LLC			Page 11
Time span=0 Runoff by SCS Reach routing by Dyn-Stor	0.00-24.00 hrs, dt=0 5 TR-20 method, UH -Ind method - Pond	.05 hrs, 481 =SCS, Weig d routing by [	points hted-CN Dyn-Stor-Ir	nd method	-
Subcatchment S101: S101	Runoff Area=12 Flow Length=427'	27,863 sf 4.59 Tc=24.9 min	9% Impervi CN=65 F	ious Runoff De Runoff=3.10 cfs	oth>1.55" 16,527 cf
Pond 1P: Ex Site Depression Discarded=0.30	Peak Elev=262 cfs 11,188 cf Prima	2.04' Storage= ary=2.18 cfs 3	=5,073 cf ,483 cf O	Inflow=3.10 cfs utflow=2.48 cfs	16,527 cf 14,671 cf
Link AP1: Abutters			F	Inflow=2.18 cfs Primary=2.18 cfs	3,483 cf 3,483 cf

Total Runoff Area = 127,863 sf Runoff Volume = 16,527 cfAverage Runoff Depth = 1.55"95.41% Pervious = 121,988 sf4.59% Impervious = 5,875 sf

#### Summary for Subcatchment S101: S101

Runoff = 3.10 cfs @ 12.38 hrs, Volume= Routed to Pond 1P : Ex Site Depression 16,527 cf, Depth> 1.55"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.86"

_	A	rea (sf)	CN D	escription					
*		98,934	68 C	)pen space	e, such as l	awns, parks, and cemeteries, HSG A			
*		16,689	30 V	0 Woods and forest, HSG A					
		5,875	98 F	aved park	ing, HSG A				
_		6,365	72 D	)irt roads, I	HSG A				
	1	27,863	65 V	Veighted A	verage				
	1	21,988	9	5.41% Per	vious Area				
		5,875	4	.59% Impe	ervious Area	а			
	_				•	<b>–</b> 1 <i>– –</i>			
		Length	Slope	Velocity	Capacity	Description			
	(min)	(feet)	(ft/ft)	(ft/sec)	(CfS)				
	15.8	50	0.0110	0.05		Sheet Flow,			
	0.0	0	0.0440	0.50		Woods: Light underbrush n= 0.400 P2= 3.15"			
	0.2	6	0.0110	0.52		Shallow Concentrated Flow,			
	0 0	27	0.0110	0 72		Shallow Concentrated Flow			
	0.0	57	0.0110	0.75		Short Grass Desture Ky= 7.0 fps			
	ΛQ	54	0 0200	0 00		Shallow Concentrated Flow			
	0.5	04	0.0200	0.55		Short Grass Pasture Ky= 7.0 fps			
	0 1	12	0 0200	2 28		Shallow Concentrated Flow.			
	••••		0.0200			Unpaved Kv= 16.1 fps			
	6.3	187	0.0050	0.49		Shallow Concentrated Flow,			
						Short Grass Pasture Kv= 7.0 fps			
	0.5	38	0.0300	1.21		Shallow Concentrated Flow,			
						Short Grass Pasture Kv= 7.0 fps			
	0.3	43	0.1000	2.21		Shallow Concentrated Flow,			
						Short Grass Pasture Kv= 7.0 fps			

24.9 427 Total

#### Summary for Pond 1P: Ex Site Depression

Inflow Area	a =	127,863 sf,	4.59% In	npervious,	Inflow Depth >	1.55"	for 10-Year event
Inflow	=	3.10 cfs @	12.38 hrs,	Volume=	16,527 c	f	
Outflow	=	2.48 cfs @	12.66 hrs,	Volume=	14,671 c	f, Atten	= 20%, Lag= 17.2 min
Discarded	=	0.30 cfs @	12.65 hrs,	Volume=	11,188 c	f	-
Primary	=	2.18 cfs @	12.66 hrs,	Volume=	3,483 c	f	
Routed	to Link /	AP1 : Abutter	S				

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 262.04' @ 12.67 hrs Surf.Area= 5,452 sf Storage= 5,073 cf

Plug-Flow detention time= 165.4 min calculated for 14,671 cf (89% of inflow) Center-of-Mass det. time= 113.4 min (989.9 - 876.5)

#### Groton 40B Pre Drainage

 Type III 24-hr
 10-Year Rainfall=4.86"

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Volume	Invert	Avail.Sto	rage Storage	e Description	
#1	260.00'	5,42	22 cf Custor	n Stage Data (Pr	ismatic) Listed below (Recalc)
Elevatio (fee 260.0 261.0 262.0 262.1	n Su t) 0 0 0 0	rf.Area (sq-ft) 215 2,056 5,425 5,500	Inc.Store (cubic-feet) 0 1,136 3,741 546	Cum.Store (cubic-feet) 0 1,136 4,876 5,422	
Device	Routing	Invert	Outlet Devic	es	
#1 #2	Discarded Primary	260.00' 262.00'	2.410 in/hr E 120.0' long Head (feet) Coef. (Englis	Exfiltration over \$ x 20.0' breadth E 0.20 0.40 0.60 sh) 2.68 2.70 2.	Surface areaPhase-In= 0.01'Broad-Crested Rectangular Weir0.801.001.201.401.60702.642.632.642.64

**Discarded OutFlow** Max=0.30 cfs @ 12.65 hrs HW=262.03' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

Primary OutFlow Max=1.96 cfs @ 12.66 hrs HW=262.03' TW=0.00' (Dynamic Tailwater) ←2=Broad-Crested Rectangular Weir (Weir Controls 1.96 cfs @ 0.49 fps)

#### Summary for Link AP1: Abutters

Inflow A	Area	=	127,863 sf,	4.59% Impervious,	Inflow Depth = 0.33	for 10-Year event
Inflow	:	=	2.18 cfs @	12.66 hrs, Volume=	3,483 cf	
Primary	y :	=	2.18 cfs @	12.66 hrs, Volume=	3,483 cf, Att	ten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Groton 40B Pre Drainage	Type III 24-hr 25-Year Rainfall=5.92"
Prepared by Howard Stein Hudson Associates	Printed 4/17/2024
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Time span=0.00-24.00 hrs, dt=0.05 hr Runoff by SCS TR-20 method, UH=SCS Reach routing by Dyn-Stor-Ind method - Pond routi	s, 481 points , Weighted-CN ng by Dyn-Stor-Ind method

Subcatchment S101: S101	Runoff Area=127,863 sf 4.59% Impervious Runoff Depth>2.28" Flow Length=427' Tc=24.9 min CN=65 Runoff=4.70 cfs 24,292 cf
Pond 1P: Ex Site Depression Discarded=0.31 of	Peak Elev=262.06' Storage=5,192 cf Inflow=4.70 cfs 24,292 cf cfs 12,173 cf Primary=4.49 cfs 9,576 cf Outflow=4.79 cfs 21,750 cf
Link AP1: Abutters	Inflow=4.49 cfs  9,576 cf Primary=4.49 cfs  9,576 cf

Total Runoff Area = 127,863 sf Runoff Volume = 24,292 cfAverage Runoff Depth = 2.28"95.41% Pervious = 121,988 sf4.59% Impervious = 5,875 sf

#### Summary for Subcatchment S101: S101

Runoff = 4.70 cfs @ 12.37 hrs, Volume= Routed to Pond 1P : Ex Site Depression 24,292 cf, Depth> 2.28"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.92"

_	A	rea (sf)	CN D	escription					
*		98,934	68 C	)pen space	e, such as l	awns, parks, and cemeteries, HSG A			
*		16,689	30 V	30 Woods and forest, HSG A					
		5,875	98 F	aved park	ing, HSG A	N Contraction of the second			
		6,365	72 C	)irt roads, l	HSG A				
	1	27,863	65 V	Veighted A	verage				
	1	21,988	9	5.41% Per	vious Area				
		5,875	4	.59% Impe	ervious Area	а			
	То	Longth	Slope	Valaaity	Conocity	Description			
	(min)	(feet)	310pe (ft/ft)	(ft/sec)	Capacity (cfs)	Description			
	15.9		0.0110	0.05	(013)	Shoot Flow			
	15.0	50	0.0110	0.05		Woods: Light underbrush $n=0.400$ P2= 3.15"			
	0.2	6	0.0110	0.52		Shallow Concentrated Flow.			
		-				Woodland Kv= 5.0 fps			
	0.8	37	0.0110	0.73		Shallow Concentrated Flow,			
						Short Grass Pasture Kv= 7.0 fps			
	0.9	54	0.0200	0.99		Shallow Concentrated Flow,			
						Short Grass Pasture Kv= 7.0 fps			
	0.1	12	0.0200	2.28		Shallow Concentrated Flow,			
	6.2	107	0.0050	0.40		Unpaved KV= 16.1 fps			
	0.3	107	0.0050	0.49		Sharlow Concentrated Flow,			
	05	38	0 0300	1 21		Shallow Concentrated Flow			
	0.0	00	0.0000	1.21		Short Grass Pasture Kv= 7.0 fps			
	0.3	43	0.1000	2.21		Shallow Concentrated Flow,			
		-				Short Grass Pasture Kv= 7.0 fps			
_									

24.9 427 Total

#### Summary for Pond 1P: Ex Site Depression

[90] Warning: Qout>Qin may require smaller dt or Finer Routing

127,863 sf, 4.59% Impervious, Inflow Depth > 2.28" for 25-Year event Inflow Area = Inflow = 4.70 cfs @ 12.37 hrs, Volume= 24,292 cf 4.79 cfs @ 12.46 hrs, Volume= Outflow = 21,750 cf, Atten= 0%, Lag= 5.4 min 0.31 cfs @ 12.45 hrs, Volume= 12,173 cf Discarded = 4.49 cfs @ 12.46 hrs, Volume= 9.576 cf Primarv = Routed to Link AP1 : Abutters

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Peak Elev= 262.06' @ 12.46 hrs Surf.Area= 5,468 sf Storage= 5,192 cf

Plug-Flow detention time= 121.3 min calculated for 21,704 cf (89% of inflow) Center-of-Mass det. time= 72.6 min (937.6 - 865.0)

Volume	Invert	Avail.Sto	rage Storage I	Description	
#1	260.00'	5,42	22 cf Custom	Stage Data (Pri	smatic) Listed below (Recalc)
Elevatio	on Su et)	ırf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
260.0	00	215	0	0	
261.0	00	2,056	1,136	1,136	
262.0	00	5,425	3,741	4,876	
262.1	10	5,500	546	5,422	
Device	Routing	Invert	Outlet Devices	6	
#1	Discarded	260.00'	2.410 in/hr Ex	filtration over S	Surface area Phase-In= 0.01'
#2	Primary	262.00'	120.0' long x	20.0' breadth B	road-Crested Rectangular Weir
	-		Head (feet) 0.	20 0.40 0.60 (	0.80 1.00 1.20 1.40 1.60
			Coef. (English	) 2.68 2.70 2.7	70 2.64 2.63 2.64 2.64 2.63

**Discarded OutFlow** Max=0.31 cfs @ 12.45 hrs HW=262.06' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.31 cfs)

Primary OutFlow Max=4.40 cfs @ 12.46 hrs HW=262.06' TW=0.00' (Dynamic Tailwater) ←2=Broad-Crested Rectangular Weir (Weir Controls 4.40 cfs @ 0.64 fps)

#### Summary for Link AP1: Abutters

Inflow A	rea =		127,863 sf,	4.59% In	npervious,	Inflow Depth =	0.90"	for 25	-Year event
Inflow	=	4	.49 cfs @	12.46 hrs,	Volume=	9,576 c	f		
Primary	/ =	4	.49 cfs @	12.46 hrs,	Volume=	9,576 c	f, Atten	= 0%,	Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Groton 40B Pre Drainage	Type III 24-hr 1	00-Year Rainfall=7.56"
Prepared by Howard Stein Hudson As	ssociates	Printed 4/17/2024
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Time span=0	.00-24.00 hrs, dt=0.05 hrs, 481 points	
Runoff by SCS	TR-20 method, UH=SCS, Weighted-CN	
Reach routing by Dyn-Stor-	Ind method - Pond routing by Dyn-Stor-I	nd method
Subcatchment S101: S101	Runoff Area=127,863 sf 4.59% Imperv	vious Runoff Depth>3.52"
	Flow Length=427' Tc=24.9 min CN=65	Runoff=7.41 cfs 37,535 cf
Pond 1P: Ex Site Depression	Peak Elev=262.08' Storage=5,312 cf	Inflow=7.41 cfs 37,535 cf
Discarded=0.31 cf	s 13,291 cf Primary=7.26 cfs 20,740 cf C	outflow=7.57 cfs 34,031 cf
Link AP1: Abutters		Inflow=7.26 cfs 20,740 cf
	P	rimary=7.26 cfs 20,740 cf
Total Runoff Area = 127,86	3 sf Runoff Volume = 37,535 cf Avera	ge Runoff Depth = 3.52"
	95.41% Pervious = 121,988 sf 4.59	% Impervious = 5,875 sf

#### Summary for Subcatchment S101: S101

Runoff = 7.41 cfs @ 12.36 hrs, Volume= Routed to Pond 1P : Ex Site Depression 37,535 cf, Depth> 3.52"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=7.56"

	A	rea (sf)	CN D	escription		
*		98,934	68 C	)pen space	e, such as l	awns, parks, and cemeteries, HSG A
*		16,689	30 V	Voods and	forest, HS	GA
		5,875	98 F	aved park	ing, HSG A	
		6,365	72 D	)irt roads, l	HSG A	
	1	27,863	65 V	Veighted A	verage	
	1	21,988	9	5.41% Per	vious Area	
		5,875	4	.59% Impe	ervious Area	а
	<b>–</b>	1 41		V/-1	0	
	IC (min)	Length			Capacity	Description
	(mm) 45.0				(CIS)	
	15.8	50	0.0110	0.05		Sheet Flow,
	0.2	6	0.0110	0.52		Shallow Concentrated Flow
	0.2	0	0.0110	0.52		Woodland Ky= 5.0 fps
	0.8	37	0.0110	0 73		Shallow Concentrated Flow
	0.0	01	0.0110	0.70		Short Grass Pasture Ky= 7.0 fps
	0.9	54	0.0200	0.99		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	0.1	12	0.0200	2.28		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
	6.3	187	0.0050	0.49		Shallow Concentrated Flow,
	_					Short Grass Pasture Kv= 7.0 fps
	0.5	38	0.0300	1.21		Shallow Concentrated Flow,
	0.0	10	0 4000	0.04		Short Grass Pasture Kv= 7.0 tps
	0.3	43	0.1000	2.21		Shallow Concentrated Flow,
						Short Grass Pasture KV= 7.0 tps

24.9 427 Total

#### Summary for Pond 1P: Ex Site Depression

[90] Warning: Qout>Qin may require smaller dt or Finer Routing

127,863 sf, 4.59% Impervious, Inflow Depth > 3.52" for 100-Year event Inflow Area = Inflow = 7.41 cfs @ 12.36 hrs, Volume= 37,535 cf 7.57 cfs @ 12.36 hrs, Volume= Outflow = 34,031 cf, Atten= 0%, Lag= 0.4 min 0.31 cfs @ 12.36 hrs, Volume= Discarded = 13,291 cf 7.26 cfs @ 12.36 hrs, Volume= 20,740 cf Primarv = Routed to Link AP1 : Abutters

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Peak Elev= 262.08' @ 12.36 hrs Surf.Area= 5,485 sf Storage= 5,312 cf

Plug-Flow detention time= 84.2 min calculated for 33,960 cf (90% of inflow) Center-of-Mass det. time= 39.8 min ( 892.2 - 852.4 )

Volume	Invert	Avail.Sto	rage Storage [	Description	
#1	260.00'	5,42	22 cf Custom	Stage Data (Pri	smatic) Listed below (Recalc)
Elevatio	on Su et)	ırf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
260.0	00	215	0	0	
261.0	00	2,056	1,136	1,136	
262.0	00	5,425	3,741	4,876	
262.1	0	5,500	546	5,422	
Device	Routing	Invert	Outlet Devices	i	
#1	Discarded	260.00'	2.410 in/hr Ex	filtration over S	Surface area Phase-In= 0.01'
#2	Primary	262.00'	120.0' long x	20.0' breadth B	road-Crested Rectangular Weir
	-		Head (feet) 0.	20 0.40 0.60 (	0.80 1.00 1.20 1.40 1.60
			Coef. (English)	) 2.68 2.70 2.7	70 2.64 2.63 2.64 2.64 2.63

**Discarded OutFlow** Max=0.31 cfs @ 12.36 hrs HW=262.08' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.31 cfs)

Primary OutFlow Max=7.16 cfs @ 12.36 hrs HW=262.08' TW=0.00' (Dynamic Tailwater) ←2=Broad-Crested Rectangular Weir (Weir Controls 7.16 cfs @ 0.75 fps)

#### Summary for Link AP1: Abutters

Inflow /	Area	a =	127,863 :	sf, 4.59% l	mpervious,	Inflow Depth =	1.95"	for 10	0-Year event
Inflow		=	7.26 cfs @	) 12.36 hrs,	Volume=	20,740 c	f		
Primar	у	=	7.26 cfs @	) 12.36 hrs,	Volume=	20,740 c	f, Atte	en= 0%,	Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

# Stage-Area-Storage for Pond 1P: Ex Site Depression

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
260.00	215	0
260.00	307	13
260.00	300	31
260.10	/01	53
260.10	583	80
260.20	675	111
260.20	767	1/7
260.30	859	188
260.00	951	233
260.40	1 043	283
260.40	1,040	338
260.55	1 228	397
260.60	1,220	460
260.65	1 412	529
260.00	1 504	602
260.75	1,596	679
260.80	1,688	761
260.85	1,780	848
260.90	1.872	939
260.95	1.964	1.035
261.00	2.056	1,136
261.05	2,224	1,243
261.10	2,393	1,358
261.15	2,561	1,482
261.20	2,730	1,614
261.25	2,898	1,755
261.30	3,067	1,904
261.35	3,235	2,061
261.40	3,404	2,227
261.45	3,572	2,402
261.50	3,741	2,585
261.55	3,909	2,776
261.60	4,077	2,976
261.65	4,246	3,184
261.70	4,414	3,400
261.75	4,583	3,625
261.80	4,751	3,858
261.85	4,920	4,100
261.90	5,088	4,350
261.95	5,257	4,609
262.00	5,425	4,876
262.05	5,463	5,148
262.10	5,500	5,422

![](_page_63_Figure_0.jpeg)

#### **Project Notes**

Rainfall events imported from "NRCS-Rain.txt" for 4253 MA Rowley Essex County Rainfall events imported from "NRCS-Rain.txt" for 4114 MA Groton Middlesex County North Rainfall events imported from "TP-40-Rain.txt" for 444 MA Middlesex

Event#	Event	Storm Type	Curve	Mode	Duration	B/B	Depth	AMC
	Name				(hours)		(inches)	
1	2-Year	Type III 24-hr		Default	24.00	1	3.15	2
2	10-Year	Type III 24-hr		Default	24.00	1	4.86	2
3	25-Year	Type III 24-hr		Default	24.00	1	5.92	2
4	100-Year	Type III 24-hr		Default	24.00	1	7.56	2

#### Rainfall Events Listing (selected events)

#### Area Listing (all nodes)

Area	CN	Description
(sq-ft)		(subcatchment-numbers)
6,949	98	Concrete, HSG A (S201, S202, S203, S204, S206, S207)
68,804	68	Open space, such as lawns, parks, and cemeteries, HSG A (S201, S202, S203,
		S204, S205, S206, S207)
24,983	98	Paved parking, HSG A (S202, S203)
13,476	98	Roofs, HSG A (B1, B2, S201, S202)
13,651	43	Woods and forest that is selectively cleared, HSG A (S201)
127,863	76	TOTAL AREA

#### Soil Listing (all nodes)

Area	Soil	Subcatchment
(sq-ft)	Group	Numbers
127,863	HSG A	B1, B2, S201, S202, S203, S204, S205, S206, S207
0	HSG B	
0	HSG C	
0	HSG D	
0	Other	
127,863		TOTAL AREA

## Groton 40B Post Drainage

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HSG-A (sq-ft)	HSG-B (sq-ft)	HSG-C (sq-ft)	HSG-D (sq-ft)	Other (sq-ft)	Total (sq-ft)	Ground Cover
6,949	0	0	0	0	6,949	Concrete
68,804	0	0	0	0	68,804	Open space, such as lawns, parks, and cemeteries
24,983	0	0	0	0	24,983	Paved parking
13,476	0	0	0	0	13,476	Roofs
13,651	0	0	0	0	13,651	Woods and forest that is selectively cleared
127,863	0	0	0	0	127,863	TOTAL AREA

#### Ground Covers (all nodes)

	Groton	40B	Post	Drainage
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Line#	Node	In-Invert	Out-Invert	Length	Slope	n	Width	Diam/Height	Inside-Fill	Node
	Number	(feet)	(feet)	(feet)	(ft/ft)		(inches)	(inches)	(inches)	Name
1	PP	262.05	261.75	60.0	0.0050	0.013	0.0	4.0	0.0	
2	YD1	261.50	261.18	65.0	0.0049	0.013	0.0	12.0	0.0	
3	YD2	261.18	261.04	28.0	0.0050	0.013	0.0	12.0	0.0	
4	YD3	261.04	260.99	10.0	0.0050	0.013	0.0	12.0	0.0	
5	YD4	262.50	262.31	39.0	0.0049	0.013	0.0	6.0	0.0	
6	YD5	262.31	262.25	12.0	0.0050	0.013	0.0	6.0	0.0	

#### Pipe Listing (all nodes)

 Line#	Node Number	Notes
 1	Project	Rainfall events imported from "NRCS-Rain.txt" for 4253 MA Rowley Essex County
2		Rainfall events imported from "NRCS-Rain.txt" for 4114 MA Groton Middlesex County North
3		Rainfall events imported from "TP-40-Rain.txt" for 444 MA Middlesex

#### Notes Listing (all nodes)

Groton 40B Post Drainag	e	Type III 24-hr 2-Year Rainfall=3.15"
Prepared by Howard Stein H	ludson Associates	Printed 4/17/2024
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Time Runc Reach routing by	e span=0.00-24.00 hrs, dt=0.05 hrs, off by SCS TR-20 method, UH=SCS, v Dyn-Stor-Ind method - Pond routir	481 points x 3 , Weighted-CN ng by Dyn-Stor-Ind method
Subcatchment B1: Building 1	Roof Runoff Area=6,581 sf	100.00% Impervious Runoff Depth>2.92" 6.0 min CN=98 Runoff=0.45 cfs 1,599 cf
Subcatchment B2: Building 2	Roof Runoff Area=6,581 sf	100.00% Impervious Runoff Depth>2.92" 6.0 min CN=98 Runoff=0.45 cfs 1,599 cf
Subcatchment S201: to Infiltr	ation Pond Runoff Area=64,556 s Flow Length=509' Tc=26	sf 1.46% Impervious Runoff Depth>0.49" 6.1 min CN=63 Runoff=0.38 cfs 2,650 cf
Subcatchment S202: to Porou	<b>Is Pavement</b> Runoff Area=24,239 sf Tc=790	f 83.36% Impervious Runoff Depth>1.19" 0.0 min CN=93 Runoff=0.10 cfs 2,404 cf
Subcatchment S203: to YD-1	Runoff Area=22,809 sf Tc=6	f 45.71% Impervious Runoff Depth>1.50" 6.0 min CN=82 Runoff=0.90 cfs 2,845 cf
Subcatchment S204: to YD-2	Runoff Area=627 sf T	f 30.62% Impervious Runoff Depth>1.17" Гс=6.0 min CN=77 Runoff=0.02 cfs 61 cf
Subcatchment S205: to YD-3	Runoff Area=605 s T	sf 0.00% Impervious Runoff Depth>0.70" Гс=6.0 min CN=68 Runoff=0.01 cfs 36 cf
Subcatchment S206: to YD-4	Runoff Area=1,101 sf Tc	f 33.88% Impervious Runoff Depth>1.24" c=6.0 min CN=78 Runoff=0.04 cfs 113 cf
Subcatchment S207: to YD-5	Runoff Area=764 sf T	f 14.27% Impervious Runoff Depth>0.90" Fc=6.0 min CN=72 Runoff=0.02 cfs 57 cf
Pond DP1: Ex Site Depressio	n Peak Elev=260.88' Discarded=0.10 cfs 2,587 cf Primary	' Storage=754 cf Inflow=0.38 cfs 2,650 cf y=0.00 cfs 0 cf Outflow=0.10 cfs 2,587 cf
Pond PP: Porous Pavement	Peak Elev=261.08 Discarded=0.65 cfs 8,706 cf Primary	' Storage=937 cf Inflow=1.88 cfs 8,714 cf y=0.00 cfs 0 cf Outflow=0.65 cfs 8,706 cf
Pond YD1: YD-1	Pe 12.0" Round Culvert n=0.013 L=65.	eak Elev=262.15' Inflow=0.90 cfs 2,845 cf .0' S=0.0049 '/' Outflow=0.90 cfs 2,845 cf
Pond YD2: YD-2	Pe 12.0" Round Culvert n=0.013 L=28.	eak Elev=261.85' Inflow=0.92 cfs 2,906 cf .0' S=0.0050 '/' Outflow=0.92 cfs 2,906 cf
Pond YD3: YD-3	Pe 12.0" Round Culvert n=0.013 L=10.	eak Elev=261.65' Inflow=0.93 cfs 2,941 cf .0' S=0.0050 '/' Outflow=0.93 cfs 2,941 cf
Pond YD4: YD-4	6.0" Round Culvert n=0.013 L=3	Peak Elev=262.65' Inflow=0.04 cfs 113 cf 39.0' S=0.0049 '/' Outflow=0.04 cfs 113 cf
Pond YD5: YD-5	6.0" Round Culvert n=0.013 L=1	Peak Elev=262.47' Inflow=0.05 cfs 171 cf 12.0' S=0.0050 '/' Outflow=0.05 cfs 171 cf
#### Link AP1: AP1

Inflow=0.00 cfs 0 cf Primary=0.00 cfs 0 cf

# Total Runoff Area = 127,863 sf Runoff Volume = 11,364 cfAverage Runoff Depth = 1.07"64.49% Pervious = 82,455 sf35.51% Impervious = 45,408 sf

#### Summary for Subcatchment B1: Building 1 Roof

Runoff = 0.45 cfs @ 12.09 hrs, Volume= 1,599 cf, Depth> 2.92" Routed to Pond PP : Porous Pavement

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.15"

Ar	ea (sf)	CN	Description				
	6,581	98	Roofs, HSC	θA			
	6,581	100.00% Impervious Area					
Tc (min)	Length (feet)	Slop (ft/ft	e Velocity ) (ft/sec)	Capacity (cfs)	Description		
6.0					Direct Entry,		

#### Summary for Subcatchment B2: Building 2 Roof

Runoff = 0.45 cfs @ 12.09 hrs, Volume= Routed to Pond PP : Porous Pavement 1,599 cf, Depth> 2.92"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.15"

Ar	ea (sf)	CN	Description					
	6,581	98	Roofs, HSG	βA				
	6,581	100.00% Impervious Area						
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
6.0					Direct Entry,			

# Summary for Subcatchment S201: to Infiltration Pond

Runoff = 0.38 cfs @ 12.48 hrs, Volume= 2,650 cf, Depth> 0.49" Routed to Pond DP1 : Ex Site Depression

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.15"

	Area (sf)	CN	Description
*	13,651	43	Woods and forest that is selectively cleared, HSG A
*	49,964	68	Open space, such as lawns, parks, and cemeteries, HSG A
*	755	98	Concrete, HSG A
	186	98	Roofs, HSG A
	64,556	63	Weighted Average
	63,615		98.54% Pervious Area
	941		1.46% Impervious Area

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
16.4	50	0.0100	0.05		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.15"
1.7	70	0.0100	0.70		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
1.0	59	0.0200	0.99		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
0.0	5	0.0150	2.49		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
6.5	275	0.0100	0.70		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
0.5	50	0.0600	1.71		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps

26.1 509 Total

#### Summary for Subcatchment S202: to Porous Pavement

Runoff = 0.10 cfs @ 21.96 hrs, Volume= Routed to Pond PP : Porous Pavement 2,404 cf, Depth> 1.19"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.15"

	Area (sf)	CN	Description						
	16,526	98	Paved park	ing, HSG A					
*	4,034	68	Open space	Open space, such as lawns, parks, and cemeteries, HSG A					
	128	98	Roofs, HSC	θA					
*	3,551	98	Concrete, H	Concrete, HSG A					
	24,239	93	Weighted A	verage					
	4,034		16.64% Pe	rvious Area					
	20,205		83.36% lm	pervious Are	ea				
(r	Tc Length nin) (feet)	Slop (ft/f	e Velocity t) (ft/sec)	Capacity (cfs)	Description				
79	90.0				Direct Entry, Extended TC based on 41" Section				
			0						

# Summary for Subcatchment S203: to YD-1

Runoff = 0.90 cfs @ 12.09 hrs, Volume= 2,845 cf, Depth> 1.50" Routed to Pond YD1 : YD-1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.15"

Type III 24-hr 2-Year Rainfall=3.15" Printed 4/17/2024 LLC Page 13

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	Area (sf)	CN	Description							
*	12,383	68	Open space	Dpen space, such as lawns, parks, and cemeteries, HSG A						
	8,457	98	Paved park	ing, HSG A	A					
*	1,969	98	Concrete, H	Concrete, HSG A						
	22,809	22.809 82 Weighted Average								
	12,383		54.29% Per	rvious Area	3					
	10,426		45.71% lmp	pervious Ar	rea					
(m	Tc Length hin) (feet)	Slope (ft/ft	e Velocity ) (ft/sec)	Capacity (cfs)	Description					
(	6.0				Direct Entry,					

#### Summary for Subcatchment S204: to YD-2

Runoff = 0.02 cfs @ 12.10 hrs, Volume= Routed to Pond YD2 : YD-2 61 cf, Depth> 1.17"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.15"

	Area (sf)	CN	Description				
*	435	68	Open space, such as lawns, parks, and cemeteries, HSG A				
*	192	98	Concrete, HSG A				
	627	77	Weighted Average				
	435		69.38% Pervious Area				
	192		30.62% Impervious Area				
-	Tc Length	Slop	pe Velocity Capacity Description				
(mi	n) (feet)	(ft/	ft) (ft/sec) (cfs)				
-	-						

6.0

Direct Entry,

#### Summary for Subcatchment S205: to YD-3

Runoff = 0.01 cfs @ 12.11 hrs, Volume= 36 cf, Depth> 0.70" Routed to Pond YD3 : YD-3

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.15"

	Area (sf)	CN	Description						
*	605	68	Open space, such as lawns, parks, and cemeteries, HSG A						
	605		100.00% Pervious Area						
Тс	: Length	Slope	e Velocity	Capacity	Description				
(min)	) (feet)	(ft/ft	) (ft/sec)	(cfs)					
6.0	)				Direct Entry,				

#### Summary for Subcatchment S206: to YD-4

Runoff = 0.04 cfs @ 12.10 hrs, Volume= 113 cf, Depth> 1.24" Routed to Pond YD4 : YD-4

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.15"

	Area (sf)	CN	Description					
*	728	68	Open space	e, such as la	awns, parks, and cemeteries, HSG A			
*	373	98	Concrete, H	ISG A	-			
	1,101 728 373	78	Weighted A 66.12% Per 33.88% Imp	Weighted Average 36.12% Pervious Area 33.88% Impervious Area				
۲ mi)	Гс Length n) (feet)	Slop (ft/f	e Velocity t) (ft/sec)	Capacity (cfs)	Description			
6	.0		· · · ·	, , , , , , , , , , , , , , , , , , ,	Direct Entry,			

#### Summary for Subcatchment S207: to YD-5

Runoff = 0.02 cfs @ 12.10 hrs, Volume= Routed to Pond YD5 : YD-5 57 cf, Depth> 0.90"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.15"

	Area (sf)	CN	Description						
*	655	68	Open space	e, such as l	lawns, parks, and cemeteries, HSG A				
*	109	98	Concrete, H	Concrete, HSG A					
	764	72	Weighted A	Veighted Average					
	655		85.73% Pervious Area						
	109		14.27% Im	pervious Ar	rea				
To (min	c Length	Slop	e Velocity	Capacity	Description				
	) (leel)	(11/1	.) (II/sec)	(CIS)					
6.0	)				Direct Entry,				

#### Summary for Pond DP1: Ex Site Depression

127,863 sf, 35.51% Impervious, Inflow Depth > 0.25" for 2-Year event Inflow Area = 0.38 cfs @ 12.48 hrs, Volume= Inflow 2.650 cf = 2,587 cf, Atten= 74%, Lag= 79.7 min Outflow 0.10 cfs @ 13.81 hrs, Volume= = Discarded = 0.10 cfs @ 13.81 hrs, Volume= 2,587 cf 0.00 cfs @ 0.00 hrs, Volume= 0 cf Primary = Routed to Link ap1 : AP1

Peak Elev= 260.88' @ 13.81 hrs Surf.Area= 1,740 sf Storage= 754 cf

Plug-Flow detention time= 103.3 min calculated for 2,587 cf (98% of inflow) Center-of-Mass det. time= 91.4 min (1,011.4 - 920.0)

Volume	Inver	t Avail.Sto	rage Storage	Description		
#1	260.00	)' 5,97	79 cf Custom	i Stage Data (Coni	<b>c)</b> Listed below (R	lecalc)
Elevatio (fee	on S et)	Surf.Area (sg-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
260.0	00	214	0	0	214	
261.0	00	2,056	978	978	2,059	
262.0	00	5,432	3,610	4,588	5,442	
262.2	25	5,700	1,391	5,979	5,718	
Device	Routing	Invert	Outlet Device	S		
#1	Discarded	260.00'	2.410 in/hr E	xfiltration over We	etted area Phas	e-In= 0.01'
#2	Primary	262.00'	70.0' long x	5.0' breadth Broad	d-Crested Rectan	gular Weir
			Head (feet) (	0.20 0.40 0.60 0.8	80 1.00 1.20 1.4	0 1.60 1.80 2.00
			2.50 3.00 3.	50 4.00 4.50 5.00	0 5.50	
			Coef. (Englisl	h) 2.34 2.50 2.70	2.68 2.68 2.66	2.65 2.65 2.65
			2.65 2.67 2.	66 2.68 2.70 2.74	4 2.79 2.88	

**Discarded OutFlow** Max=0.10 cfs @ 13.81 hrs HW=260.88' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.10 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=260.00' TW=0.00' (Dynamic Tailwater) ←2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

#### **Summary for Pond PP: Porous Pavement**

Inflow Area	a =	63,307 sf,	70.24% Im	pervious,	Inflow Depth >	1.65"	for 2-Year event
Inflow	=	1.88 cfs @	12.09 hrs,	Volume=	8,714 cf		
Outflow	=	0.65 cfs @	12.39 hrs,	Volume=	8,706 cf,	, Atten	= 65%, Lag= 17.8 min
Discarded	=	0.65 cfs @	12.39 hrs,	Volume=	8,706 cf		-
Primary	=	0.00 cfs @	0.00 hrs,	Volume=	0 cf		
Routed	to Pond	DP1 : Ex Site	e Depressio	n			

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 261.08' @ 12.39 hrs Surf.Area= 10,986 sf Storage= 937 cf

Plug-Flow detention time= 5.5 min calculated for 8,706 cf (100% of inflow) Center-of-Mass det. time= 5.0 min (915.0 - 910.0)

Volume	Invert	Avail.Storage	Storage Description
#1	260.87'	13,002 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

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Elevatio	elevation Surf.Area		Void	s Inc.Store	Cum.Store
(fee	et)	(sq-ft)	(%	) (cubic-feet)	(cubic-feet)
260.8	37	10,986	0.	0 0	0
260.8	38	10,986	40.	) 44	44
262.3	37	10,986	40.	0 6,548	6,592
262.3	38	10,986	15.	) 16	6,608
262.6	62	10,986	15.	) 395	7,004
262.6	63	10,986	40.	) 44	7,048
263.6	63	10,986	40.	) 4,394	11,442
263.6	64	10,986	25.	) 27	11,469
263.9	96	10,986	25.	) 879	12,348
263.9	97	10,986	15.	) 16	12,365
264.29		10,986	15.	) 527	12,892
264.30		10,986	100.	D 110	13,002
Device	Routing	In	vert	Outlet Devices	
#1	Discarded	260	.87'	2.410 in/hr Exfiltrat	ion over Surface ar

#1	Discarded	260.87'	2.410 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 257.75' Phase-In= 0.01'
#2	Primary	262.05'	4.0" Round Culvert X 3.00 L= 60.0' Ke= 0.500
	-		Inlet / Outlet Invert= 262.05' / 261.75' S= 0.0050 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.09 sf

**Discarded OutFlow** Max=0.65 cfs @ 12.39 hrs HW=261.08' (Free Discharge) **1=Exfiltration** (Controls 0.65 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=260.87' TW=260.00' (Dynamic Tailwater) →2=Culvert (Controls 0.00 cfs)

# Summary for Pond YD1: YD-1

Inflow Area	a =	22,809 sf,	45.71% Im	pervious,	Inflow Depth >	1.50"	for 2-Year event
Inflow	=	0.90 cfs @	12.09 hrs, N	Volume=	2,845 ct	F	
Outflow	=	0.90 cfs @	12.09 hrs, \	/olume=	2,845 ct	, Atten	= 0%, Lag= 0.0 min
Primary	=	0.90 cfs @	12.09 hrs, \	/olume=	2,845 cf	-	
Routed	to Pond	YD2 : YD-2					

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 262.15' @ 12.09 hrs Flood Elev= 263.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	261.50'	<b>12.0" Round Culvert</b> L= 65.0' Ke= 0.500 Inlet / Outlet Invert= 261.50' / 261.18' S= 0.0049 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.89 cfs @ 12.09 hrs HW=262.15' TW=261.84' (Dynamic Tailwater) ←1=Culvert (Outlet Controls 0.89 cfs @ 2.34 fps)

# Summary for Pond YD2: YD-2

Inflow Area = 23,436 sf, 45.31% Impervious, Inflow Depth > 1.49" for 2-Year event Inflow 0.92 cfs @ 12.09 hrs, Volume= 2.906 cf = 0.92 cfs @ 12.09 hrs, Volume= Outflow 2,906 cf, Atten= 0%, Lag= 0.0 min = 2,906 cf Primary = 0.92 cfs @ 12.09 hrs, Volume= Routed to Pond YD3 : YD-3 Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 261.85' @ 12.09 hrs Flood Elev= 263.50' Device Routing Invert Outlet Devices #1 Primary 261.18' **12.0" Round Culvert** L= 28.0' Ke= 0.500 Inlet / Outlet Invert= 261.18' / 261.04' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf Primary OutFlow Max=0.90 cfs @ 12.09 hrs HW=261.84' TW=261.64' (Dynamic Tailwater)

**1=Culvert** (Outlet Controls 0.90 cfs @ 2.32 fps)

# Summary for Pond YD3: YD-3

Inflow Area	ı =	24,041 sf,	44.17% In	npervious,	Inflow Depth >	> 1	.47"	for 2-	Year ever	nt
Inflow	=	0.93 cfs @	12.09 hrs,	Volume=	2,941	cf				
Outflow	=	0.93 cfs @	12.09 hrs,	Volume=	2,941	cf,	Atten	= 0%,	Lag= 0.0	min
Primary	=	0.93 cfs @	12.09 hrs,	Volume=	2,941	cf				
Routed	to Pond	PP : Porous	Pavement							

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 261.65' @ 12.09 hrs Flood Elev= 263.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	261.04'	<b>12.0" Round Culvert</b> L= 10.0' Ke= 0.500
			Inlet / Outlet Invert= 261.04' / 260.99' S= 0.0050 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.91 cfs @ 12.09 hrs HW=261.64' TW=260.98' (Dynamic Tailwater) -1=Culvert (Barrel Controls 0.91 cfs @ 2.65 fps)

# Summary for Pond YD4: YD-4

Inflow Area	a =	1,101 sf,	33.88% Im	pervious,	Inflow Depth >	1.24"	for 2-	Year event
Inflow	=	0.04 cfs @	12.10 hrs,	Volume=	113 c	f		
Outflow	=	0.04 cfs @	12.10 hrs,	Volume=	113 c	f, Atte	n= 0%,	Lag= 0.0 min
Primary	=	0.04 cfs @	12.10 hrs,	Volume=	113 c	f		-
Routed	to Pond	YD5 : YD-5						

Peak Elev= 262.65' @ 12.10 hrs Flood Elev= 264.50'

DeviceRoutingInvertOutlet Devices#1Primary262.50'6.0" Round CulvertL= 39.0'Ke= 0.500Inlet / Outlet Invert=262.50'/ 262.31'S= 0.0049 '/'Cc= 0.900n= 0.013Corrugated PE, smooth interior, Flow Area=0.20 sf

**Primary OutFlow** Max=0.03 cfs @ 12.10 hrs HW=262.64' TW=262.47' (Dynamic Tailwater) **1=Culvert** (Outlet Controls 0.03 cfs @ 1.11 fps)

#### Summary for Pond YD5: YD-5

Inflow Area =1,865 sf, 25.84% Impervious, Inflow Depth >1.10" for 2-Year eventInflow =0.05 cfs @12.10 hrs, Volume=171 cfOutflow =0.05 cfs @12.10 hrs, Volume=171 cf, Atten= 0%, Lag= 0.0 minPrimary =0.05 cfs @12.10 hrs, Volume=171 cfRouted to Pond PP : Porous Pavement171 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 262.47' @ 12.10 hrs Flood Elev= 264.50'

DeviceRoutingInvertOutlet Devices#1Primary262.31'6.0" Round CulvertL= 12.0'Ke= 0.500Inlet / Outlet Invert=262.31' / 262.25'S= 0.0050 '/'Cc= 0.900n= 0.013Corrugated PE, smooth interior, Flow Area=0.20 sf

Primary OutFlow Max=0.05 cfs @ 12.10 hrs HW=262.47' TW=260.98' (Dynamic Tailwater) ←1=Culvert (Barrel Controls 0.05 cfs @ 1.37 fps)

#### Summary for Link AP1: AP1

Inflow A	rea =	127,863 sf,	35.51% Impervious,	Inflow Depth = 0.00"	for 2-Year event
Inflow	=	0.00 cfs @	0.00 hrs, Volume=	0 cf	
Primary	=	0.00 cfs @	0.00 hrs, Volume=	0 cf, Atter	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Groton 40B Post Drainage Prepared by Howard Stein Hudson Asso HydroCAD® 10.20-4a s/n 02930 © 2023 Hydr	Type III 24-hr 10-Year Rainfall=4.86"ociatesPrinted 4/17/2024ocAD Software Solutions LLCPage 19
Time span=0.00-2 Runoff by SCS TF Reach routing by Dyn-Stor-Inc	24.00 hrs, dt=0.05 hrs, 481 points x 3 -20 method, UH=SCS, Weighted-CN I method - Pond routing by Dyn-Stor-Ind method
Subcatchment B1: Building 1 Roof	Runoff Area=6,581 sf 100.00% Impervious Runoff Depth>4.62" Tc=6.0 min CN=98 Runoff=0.70 cfs 2,534 cf
Subcatchment B2: Building 2 Roof	Runoff Area=6,581 sf 100.00% Impervious Runoff Depth>4.62" Tc=6.0 min CN=98 Runoff=0.70 cfs 2,534 cf
Subcatchment S201: to Infiltration Pond	Runoff Area=64,556 sf 1.46% Impervious Runoff Depth>1.41" low Length=509' Tc=26.1 min CN=63 Runoff=1.37 cfs 7,590 cf
Subcatchment S202: to Porous Pavement	Runoff Area=24,239 sf 83.36% Impervious Runoff Depth>2.07" Tc=790.0 min CN=93 Runoff=0.16 cfs 4,184 cf
Subcatchment S203: to YD-1	Runoff Area=22,809 sf 45.71% Impervious Runoff Depth>2.95" Tc=6.0 min CN=82 Runoff=1.77 cfs 5,610 cf
Subcatchment S204: to YD-2	Runoff Area=627 sf 30.62% Impervious Runoff Depth>2.50" Tc=6.0 min CN=77 Runoff=0.04 cfs 131 cf
Subcatchment S205: to YD-3	Runoff Area=605 sf 0.00% Impervious Runoff Depth>1.78" Tc=6.0 min CN=68 Runoff=0.03 cfs 90 cf
Subcatchment S206: to YD-4	Runoff Area=1,101 sf 33.88% Impervious Runoff Depth>2.59" Tc=6.0 min CN=78 Runoff=0.08 cfs 238 cf
Subcatchment S207: to YD-5	Runoff Area=764 sf 14.27% Impervious Runoff Depth>2.09" Tc=6.0 min CN=72 Runoff=0.04 cfs 133 cf
Pond DP1: Ex Site Depression Discarded=0.	Peak Elev=261.68' Storage=3,068 cf Inflow=1.37 cfs 7,590 cf 23 cfs 7,075 cf Primary=0.00 cfs 0 cf Outflow=0.23 cfs 7,075 cf
Pond PP: Porous Pavement Discarded=0.74	Peak Elev=261.50' Storage=2,754 cf Inflow=3.37 cfs 15,454 cf cfs 15,440 cf Primary=0.00 cfs 0 cf Outflow=0.74 cfs 15,440 cf
Pond YD1: YD-1 12.0" Round	Peak Elev=262.55' Inflow=1.77 cfs 5,610 cf Culvert n=0.013 L=65.0' S=0.0049 '/' Outflow=1.77 cfs 5,610 cf
Pond YD2: YD-2 12.0" Round	Peak Elev=262.22' Inflow=1.81 cfs 5,741 cf Culvert n=0.013 L=28.0' S=0.0050 '/' Outflow=1.81 cfs 5,741 cf
Pond YD3: YD-3 12.0" Round	Peak Elev=261.96' Inflow=1.84 cfs 5,831 cf Culvert n=0.013 L=10.0' S=0.0050 '/' Outflow=1.84 cfs 5,831 cf
Pond YD4: YD-4 6.0" Rou	Peak Elev=262.72' Inflow=0.08 cfs 238 cf nd Culvert n=0.013 L=39.0' S=0.0049 '/' Outflow=0.08 cfs 238 cf
Pond YD5: YD-5 6.0" Rou	Peak Elev=262.56' Inflow=0.12 cfs 371 cf nd Culvert n=0.013 L=12.0' S=0.0050 '/' Outflow=0.12 cfs 371 cf

#### Link AP1: AP1

Inflow=0.00 cfs 0 cf Primary=0.00 cfs 0 cf

#### Total Runoff Area = 127,863 sf Runoff Volume = 23,044 cf Average Runoff Depth = 2.16" 64.49% Pervious = 82,455 sf 35.51% Impervious = 45,408 sf

#### Summary for Subcatchment B1: Building 1 Roof

Runoff = 0.70 cfs @ 12.09 hrs, Volume= 2,534 cf, Depth> 4.62" Routed to Pond PP : Porous Pavement

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.86"

Ar	ea (sf)	CN	Description				
	6,581	98	Roofs, HSG A				
	6,581		100.00% Impervious Area				
Tc (min)	Length (feet)	Slop (ft/ft	e Velocity ) (ft/sec)	Capacity (cfs)	Description		
6.0					Direct Entry,		

#### Summary for Subcatchment B2: Building 2 Roof

Runoff = 0.70 cfs @ 12.09 hrs, Volume= Routed to Pond PP : Porous Pavement

2,534 cf, Depth> 4.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.86"

A	rea (sf)	CN	Description				
	6,581	98	Roofs, HSC	βA			
	6,581	100.00% Impervious Area					
Tc (min)	Length (feet)	Slope (ft/ft	Velocity (ft/sec)	Capacity (cfs)	Description		
6.0					Direct Entry,		

#### Summary for Subcatchment S201: to Infiltration Pond

Runoff = 1.37 cfs @ 12.40 hrs, Volume= 7,590 cf, Depth> 1.41" Routed to Pond DP1 : Ex Site Depression

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.86"

	Area (sf)	CN	Description
*	13,651	43	Woods and forest that is selectively cleared, HSG A
*	49,964	68	Open space, such as lawns, parks, and cemeteries, HSG A
*	755	98	Concrete, HSG A
	186	98	Roofs, HSG A
	64,556	63	Weighted Average
	63,615		98.54% Pervious Area
	941		1.46% Impervious Area

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Type III 24-hr 10-Year Rainfall=4.86" Printed 4/17/2024 HydroCAD® 10.20-4a s/n 02930 © 2023 HydroCAD Software Solutions LLC Page 22

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
16.4	50	0.0100	0.05		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.15"
1.7	70	0.0100	0.70		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
1.0	59	0.0200	0.99		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
0.0	5	0.0150	2.49		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
6.5	275	0.0100	0.70		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
0.5	50	0.0600	1.71		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps

26.1 509 Total

#### Summary for Subcatchment S202: to Porous Pavement

0.16 cfs @ 21.95 hrs, Volume= Runoff = Routed to Pond PP : Porous Pavement

4,184 cf, Depth> 2.07"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.86"

	Area (sf)	CN	Description				
	16,526	98	Paved park	ing, HSG A			
*	4,034	68	Open space	e, such as l	awns, parks, and cemeteries, HSG A		
	128	98	Roofs, HSC	θA			
*	3,551	98	Concrete, H	ISG A			
	24,239	93	Weighted A	verage			
	4,034		16.64% Pervious Area				
	20,205		83.36% Im	pervious Are	ea		
(m	Tc Length in) (feet)	Slop (ft/f	e Velocity t) (ft/sec)	Capacity (cfs)	Description		
790	0.0				Direct Entry, Extended TC based on 41" Section		
			0				

### Summary for Subcatchment S203: to YD-1

5,610 cf, Depth> 2.95" Runoff 1.77 cfs @ 12.09 hrs, Volume= = Routed to Pond YD1 : YD-1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.86"

Type III 24-hr 10-Year Rainfall=4.86" Printed 4/17/2024 LC Page 23

131 cf, Depth> 2.50"

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	Area (sf)	CN	Description				
*	12,383	68	Open space	e, such as l	lawns, parks, and cemeteries, HSG A		
	8,457	98	Paved park	ing, HSG A	<i>A</i>		
*	1,969	98	Concrete, H	ISG A			
	22,809	82	Weighted A	verage			
	12,383	3 54.29% Pervious Area					
	10,426		45.71% Impervious Area				
T (miı	c Length n) (feet)	Slop (ft/f	e Velocity ) (ft/sec)	Capacity (cfs)	Description		
6	0				Direct Entry,		

#### Summary for Subcatchment S204: to YD-2

Runoff	=	0.04 cfs @	12.09 hrs,	Volume=
Routed	to Pon	d YD2 : YD-2		

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.86"

	Area (sf)	CN	Description						
*	435	68	Open space	pen space, such as lawns, parks, and cemeteries, HSG A					
*	192	98	Concrete, H	oncrete, HSG A					
	627 435	77	Weighted A 69.38% Per	Veighted Average 39.38% Pervious Area					
	192		30.62% Imp	0.62% Impervious Area					
- (mi	Гс Length n) (feet)	Slop (ft/f	e Velocity t) (ft/sec)	Capacity (cfs)	Description				
6	.0				Direct Entry.				

Direct Entry,

#### Summary for Subcatchment S205: to YD-3

0.03 cfs @ 12.10 hrs, Volume= 90 cf, Depth> 1.78" Runoff = Routed to Pond YD3 : YD-3

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.86"

	Area (sf)	CN	Description					
*	605	68	8 Open space, such as lawns, parks, and cemeteries, HSG A					
	605		100.00% Pervious Area					
Т	c Length	Slope	e Velocity	Capacity	Description			
(mir	) (feet)	(ft/ft)	(ft/sec)	(cfs)				
6.	0				Direct Entry,			

#### Summary for Subcatchment S206: to YD-4

Runoff = 0.08 cfs @ 12.09 hrs, Volume= 238 cf, Depth> 2.59" Routed to Pond YD4 : YD-4

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.86"

	Area (sf)	CN	Description					
*	728	68	Open space	e, such as la	awns, parks, and cemeteries, HSG A			
*	373	98	Concrete, H	concrete, HSG A				
	1,101 728 373	78	Weighted A 66.12% Per 33.88% Imp	verage vious Area pervious Are	ea			
۲ mi)	Гс Length n) (feet)	Slop (ft/f	e Velocity t) (ft/sec)	Capacity (cfs)	Description			
6	.0		· · · ·	, , , , , , , , , , , , , , , , , , ,	Direct Entry,			

#### Summary for Subcatchment S207: to YD-5

Runoff = 0.04 cfs @ 12.10 hrs, Volume= Routed to Pond YD5 : YD-5 133 cf, Depth> 2.09"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.86"

	Area (sf)	CN	Description						
*	655	68	Open space	e, such as l	lawns, parks, and cemeteries, HSG A				
*	109	98	Concrete, H	ISG A					
	764	72	Weighted A	verage					
	655		85.73% Pe	85.73% Pervious Area					
	109		14.27% lmp	4.27% Impervious Area					
Ţ	c Length	Slop	e Velocity	Capacity	Description				
(mir	i) (feet)	(ft/f	:) (ft/sec)	(cts)					
6.	0				Direct Entry,				

#### Summary for Pond DP1: Ex Site Depression

127,863 sf, 35.51% Impervious, Inflow Depth > 0.71" for 10-Year event Inflow Area = 1.37 cfs @ 12.40 hrs, Volume= 7,590 cf Inflow = 7,075 cf, Atten= 83%, Lag= 88.7 min Outflow 0.23 cfs @ 13.88 hrs, Volume= = Discarded = 0.23 cfs @ 13.88 hrs, Volume= 7.075 cf 0.00 cfs @ 0.00 hrs, Volume= 0 cf Primary = Routed to Link ap1 : AP1

Peak Elev= 261.68' @ 13.88 hrs Surf.Area= 4,188 sf Storage= 3,068 cf

Plug-Flow detention time= 177.6 min calculated for 7,075 cf (93% of inflow) Center-of-Mass det. time= 143.9 min (1,026.8 - 883.0)

Volume	Invert	Avail.Sto	rage Storage	Description		
#1	260.00	5,97	79 cf Custom	Stage Data (Coni	<b>c)</b> Listed below (R	ecalc)
Elevatio	on S	urf.Area	Inc.Store	Cum.Store	Wet.Area	
(tee	et)	(sq-tt)	(cubic-teet)	(CUDIC-TEET)	(sq-tt)	
260.0	00	214	0	0	214	
261.0	00	2,056	978	978	2,059	
262.0	00	5,432	3,610	4,588	5,442	
262.2	25	5,700	1,391	5,979	5,718	
Device	Routing	Invert	Outlet Device	s		
#1	Discarded	260.00'	2.410 in/hr Ex	filtration over We	tted area Phase	e-In= 0.01'
#2 Primary 262.		262.00'	70.0' long x \$	5.0' breadth Broad	I-Crested Rectang	jular Weir
	-		Head (feet) C	0.20 0.40 0.60 0.8	30 1.00 1.20 1.40	0 1.60 1.80 2.00
			2.50 3.00 3.	50 4.00 4.50 5.00	) 5.50	
			Coef. (English	n) 2.34 2.50 2.70	2.68 2.68 2.66	2.65 2.65 2.65
			2.65 2.67 2.0	66 2.68 2.70 2.74	2.79 2.88	

**Discarded OutFlow** Max=0.23 cfs @ 13.88 hrs HW=261.68' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.23 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=260.00' TW=0.00' (Dynamic Tailwater) ←2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

#### **Summary for Pond PP: Porous Pavement**

Inflow Area	a =	63,307 sf,	70.24% In	npervious,	Inflow Depth >	2.93"	for 10-	Year event
Inflow	=	3.37 cfs @	12.09 hrs,	Volume=	15,454 c	f		
Outflow	=	0.74 cfs @	12.51 hrs,	Volume=	15,440 c	f, Atter	n= 78%,	Lag= 25.3 min
Discarded	=	0.74 cfs @	12.51 hrs,	Volume=	15,440 c	f		-
Primary	=	0.00 cfs @	0.00 hrs,	Volume=	0 c	f		
Routed to Pond DP1 : Ex Site Depression								

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 261.50' @ 12.51 hrs Surf.Area= 10,986 sf Storage= 2,754 cf

Plug-Flow detention time= 16.5 min calculated for 15,408 cf (100% of inflow) Center-of-Mass det. time= 16.0 min (914.4 - 898.4)

Volume	Invert	Avail.Storage	Storage Description
#1	260.87'	13,002 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

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Elevatio	on S	urf.Area	Voids	Inc.Store	Cum.Store
(fee	et)	(sq-ft)	(%)	(cubic-feet)	(cubic-feet)
260.8	37	10,986	0.0	0	0
260.8	88	10,986	40.0	44	44
262.3	37	10,986	40.0	6,548	6,592
262.3	88	10,986	15.0	16	6,608
262.6	62	10,986	15.0	395	7,004
262.63		10,986	40.0	44	7,048
263.6	63	10,986	40.0	4,394	11,442
263.6	64	10,986	25.0	27	11,469
263.9	96	10,986	25.0	879	12,348
263.9	)7	10,986	15.0	16	12,365
264.2	29	10,986	15.0	527	12,892
264.30		10,986	100.0	110	13,002
Device	Routing	In	vert C	Outlet Devices	
#1	Discarded	260	87' <b>2</b>	410 in/hr Exfiltrat	tion over Surface ar

#1	Discarded	260.87'	2.410 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 257.75' Phase-In= 0.01'
#2	Primary	262.05'	4.0" Round Culvert X 3.00 L= 60.0' Ke= 0.500
	•		Inlet / Outlet Invert= 262.05' / 261.75' S= 0.0050 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.09 sf

**Discarded OutFlow** Max=0.74 cfs @ 12.51 hrs HW=261.50' (Free Discharge) **1=Exfiltration** (Controls 0.74 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=260.87' TW=260.00' (Dynamic Tailwater) →2=Culvert (Controls 0.00 cfs)

# Summary for Pond YD1: YD-1

Inflow Are	a =	22,809 sf,	45.71% Im	pervious,	Inflow Depth >	2.95"	for 10-Ye	ear event
Inflow	=	1.77 cfs @	12.09 hrs,	Volume=	5,610 c	f		
Outflow	=	1.77 cfs @	12.09 hrs,	Volume=	5,610 c	f, Atten	= 0%, Lag	g= 0.0 min
Primary	=	1.77 cfs @	12.09 hrs,	Volume=	5,610 c	f		
Routed	to Pond	I YD2 : YD-2						

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 262.55' @ 12.09 hrs Flood Elev= 263.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	261.50'	<b>12.0" Round Culvert</b> L= 65.0' Ke= 0.500 Inlet / Outlet Invert= 261.50' / 261.18' S= 0.0049 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=1.74 cfs @ 12.09 hrs HW=262.54' TW=262.20' (Dynamic Tailwater) ←1=Culvert (Outlet Controls 1.74 cfs @ 2.65 fps)

# Summary for Pond YD2: YD-2

Inflow Area = 23,436 sf, 45.31% Impervious, Inflow Depth > 2.94" for 10-Year event Inflow 1.81 cfs @ 12.09 hrs, Volume= 5.741 cf = 1.81 cfs @ 12.09 hrs, Volume= Outflow 5,741 cf, Atten= 0%, Lag= 0.0 min = Primary = 1.81 cfs @ 12.09 hrs, Volume= 5.741 cf Routed to Pond YD3 : YD-3 Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 262.22' @ 12.09 hrs Flood Elev= 263.50' Device Routing Invert Outlet Devices #1 Primary 261.18' **12.0" Round Culvert** L= 28.0' Ke= 0.500 Inlet / Outlet Invert= 261.18' / 261.04' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf Primary OutFlow Max=1.78 cfs @ 12.09 hrs HW=262.20' TW=261.94' (Dynamic Tailwater)

**1=Culvert** (Outlet Controls 1.78 cfs @ 2.76 fps)

# Summary for Pond YD3: YD-3

Inflow Area	ı =	24,041 sf,	44.17% In	npervious,	Inflow Depth >	2.9	91" for 10	-Year event
Inflow	=	1.84 cfs @	12.09 hrs,	Volume=	5,831	cf		
Outflow	=	1.84 cfs @	12.09 hrs,	Volume=	5,831	cf, A	Atten= 0%,	Lag= 0.0 min
Primary	=	1.84 cfs @	12.09 hrs,	Volume=	5,831	cf		-
Routed	to Pond	PP : Porous	Pavement					

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 261.96' @ 12.09 hrs Flood Elev= 263.50'

Device	Routing	Invert	Outlet Devices				
#1	Primary	261.04'	<b>12.0" Round Culvert</b> L= 10.0' Ke= 0.500				
			Inlet / Outlet Invert= 261.04' / 260.99' S= 0.0050 '/' Cc= 0.900				
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf				

**Primary OutFlow** Max=1.81 cfs @ 12.09 hrs HW=261.94' TW=261.18' (Dynamic Tailwater) **1=Culvert** (Barrel Controls 1.81 cfs @ 3.18 fps)

# Summary for Pond YD4: YD-4

Inflow Area	a =	1,101 sf,	33.88% Im	npervious,	Inflow Depth >	2.59"	for 10	-Year event
Inflow	=	0.08 cfs @	12.09 hrs,	Volume=	238 c	f		
Outflow	=	0.08 cfs @	12.09 hrs,	Volume=	238 c	f, Atter	ו= 0%,	Lag= 0.0 min
Primary	=	0.08 cfs @	12.09 hrs,	Volume=	238 c	f		-
Routed	to Pond	1 YD5 : YD-5						

Peak Elev= 262.72' @ 12.09 hrs Flood Elev= 264.50'

DeviceRoutingInvertOutlet Devices#1Primary262.50'6.0" Round CulvertL= 39.0'Ke= 0.500Inlet / Outlet Invert=262.50'/ 262.31'S= 0.0049 '/'Cc= 0.900n= 0.013Corrugated PE, smooth interior, Flow Area=0.20 sf

Primary OutFlow Max=0.07 cfs @ 12.09 hrs HW=262.72' TW=262.56' (Dynamic Tailwater) -1=Culvert (Outlet Controls 0.07 cfs @ 1.30 fps)

### Summary for Pond YD5: YD-5

Inflow Area = 1,865 sf, 25.84% Impervious, Inflow Depth > 2.39" for 10-Year event Inflow 0.12 cfs @ 12.09 hrs, Volume= 371 cf = 0.12 cfs @ 12.09 hrs, Volume= Outflow 371 cf, Atten= 0%, Lag= 0.0 min = Primary 0.12 cfs @ 12.09 hrs, Volume= = 371 cf Routed to Pond PP : Porous Pavement

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 262.56' @ 12.09 hrs Flood Elev= 264.50'

DeviceRoutingInvertOutlet Devices#1Primary262.31'6.0" Round CulvertL= 12.0'Ke= 0.500Inlet / Outlet Invert= 262.31' / 262.25'S= 0.0050 '/'Cc= 0.900n= 0.013Corrugated PE, smooth interior, Flow Area= 0.20 sf

Primary OutFlow Max=0.12 cfs @ 12.09 hrs HW=262.56' TW=261.18' (Dynamic Tailwater) -1=Culvert (Barrel Controls 0.12 cfs @ 1.70 fps)

#### Summary for Link AP1: AP1

Inflow A	rea =	127,863 sf,	35.51% Impervious,	Inflow Depth = 0.00"	for 10-Year event
Inflow	=	0.00 cfs @	0.00 hrs, Volume=	0 cf	
Primary	· =	0.00 cfs @	0.00 hrs, Volume=	0 cf, Atter	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

<b>Groton 40B Post Drainage</b> Prepared by Howard Stein Hudson Asso HydroCAD® 10 20-4a, s/p 02930, © 2023 Hydr	7 ociates oCAD Software Solutions	Type III 24-hr	25-Year Rainfall=5.92" Printed 4/17/2024
Time span=0.00-2	24.00 hrs, dt=0.05 hrs, 44	81 points x 3	nd method
Runoff by SCS TF	R-20 method, UH=SCS, V	Weighted-CN	
Reach routing by Dyn-Stor-Inc	I method - Pond routing	9 by Dyn-Stor-I	
Subcatchment B1: Building 1 Roof	Runoff Area=6,581 sf 1	100.00% Imperv	/ious Runoff Depth>5.68"
	Tc=6.	0 min CN=98	Runoff=0.86 cfs 3,114 cf
Subcatchment B2: Building 2 Roof	Runoff Area=6,581 sf 1	100.00% Imperv	vious Runoff Depth>5.68"
	Tc=6.	0 min CN=98	Runoff=0.86 cfs 3,114 cf
Subcatchment S201: to Infiltration Pond	Runoff Area=64,556 sf	1.46% Imperv	vious Runoff Depth>2.11"
	ow Length=509' Tc=26.1	min CN=63	Runoff=2.13 cfs 11,336 cf
Subcatchment S202: to Porous Pavement	Runoff Area=24,239 sf	83.36% Imperv	/ious Runoff Depth>2.63"
	Tc=790.	0 min CN=93	Runoff=0.20 cfs 5,314 cf
Subcatchment S203: to YD-1	Runoff Area=22,809 sf	45.71% Imperv	vious Runoff Depth>3.91"
	Tc=6.	0 min CN=82	Runoff=2.33 cfs 7,433 cf
Subcatchment S204: to YD-2	Runoff Area=627 sf	30.62% Imperv	vious Runoff Depth>3.41"
	Tc=	6.0 min CN=7	7 Runoff=0.06 cfs 178 cf
Subcatchment S205: to YD-3	Runoff Area=605 sf	0.00% Imperv	vious Runoff Depth>2.56"
	Tc=	6.0 min CN=6	8 Runoff=0.04 cfs 129 cf
Subcatchment S206: to YD-4	Runoff Area=1,101 sf	33.88% Imperv	vious Runoff Depth>3.51"
	Tc=	6.0 min CN=7	8 Runoff=0.10 cfs 322 cf
Subcatchment S207: to YD-5	Runoff Area=764 sf	14.27% Imperv	vious Runoff Depth>2.93"
	Tc=	6.0 min CN=7	2 Runoff=0.06 cfs 186 cf
Pond DP1: Ex Site Depression	Peak Elev=262.01' Sto	rage=4,666 cf	Inflow=2.13 cfs 11,336 cf
Discarded=0.30	ofs 9,820 cf Primary=0.24	8 cfs  471 cf   C	Dutflow=0.59 cfs 10,291 cf
Pond PP: Porous Pavement	Peak Elev=261.79' Sto	rage=4,025 cf	Inflow=4.31 cfs 19,790 cf
Discarded=0.79	cfs 19,774 cf Primary=0	).00 cfs 0 cf C	Dutflow=0.79 cfs 19,774 cf
Pond YD1: YD-1	Pea	ak Elev=263.03'	Inflow=2.33 cfs 7,433 cf
12.0" Round	Culvert n=0.013 L=65.0	' S=0.0049 '/'	Outflow=2.33 cfs 7,433 cf
Pond YD2: YD-2	Pea	ak Elev=262.55'	Inflow=2.39 cfs 7,611 cf
12.0" Round	1 Culvert n=0.013 L=28.0	' S=0.0050 '/'	Outflow=2.39 cfs 7,611 cf
Pond YD3: YD-3	Pea	ak Elev=262.15'	Inflow=2.43 cfs 7,740 cf
12.0" Round	1 Culvert n=0.013 L=10.0	' S=0.0050 '/'	Outflow=2.43 cfs 7,740 cf
Pond YD4: YD-4 6.0" Rou	Po	eak Elev=262.7	7' Inflow=0.10 cfs 322 cf
	nd Culvert n=0.013 L=39	.0' S=0.0049 '/'	Outflow=0.10 cfs 322 cf
<b>Pond YD5: YD-5</b> 6.0" Rou	Po	eak Elev=262.6	1' Inflow=0.16 cfs 508 cf
	nd Culvert n=0.013 L=12	.0' S=0.0050 '/'	Outflow=0.16 cfs 508 cf

#### Link AP1: AP1

Inflow=0.28 cfs 471 cf Primary=0.28 cfs 471 cf

#### Total Runoff Area = 127,863 sf Runoff Volume = 31,126 cf Average Runoff Depth = 2.92" 64.49% Pervious = 82,455 sf 35.51% Impervious = 45,408 sf

#### Summary for Subcatchment B1: Building 1 Roof

Runoff = 0.86 cfs @ 12.09 hrs, Volume= Routed to Pond PP : Porous Pavement

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.92"

Ar	ea (sf)	CN	Description					
	6,581	98	Roofs, HSC	θA				
	6,581		100.00% Impervious Area					
Tc (min)	Length (feet)	Slop (ft/ft	e Velocity ) (ft/sec)	Capacity (cfs)	Description			
6.0					Direct Entry,			

#### Summary for Subcatchment B2: Building 2 Roof

Runoff = 0.86 cfs @ 12.09 hrs, Volume= Routed to Pond PP : Porous Pavement 3,114 cf, Depth> 5.68"

3,114 cf, Depth> 5.68"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.92"

A	rea (sf)	CN	Description						
	6,581	98	Roofs, HSG A						
	6,581		100.00% Impervious Area						
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
6.0					Direct Entry,				

#### Summary for Subcatchment S201: to Infiltration Pond

Runoff = 2.13 cfs @ 12.39 hrs, Volume= 11,336 cf, Depth> 2.11" Routed to Pond DP1 : Ex Site Depression

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.92"

	Area (sf)	CN	Description
*	13,651	43	Woods and forest that is selectively cleared, HSG A
*	49,964	68	Open space, such as lawns, parks, and cemeteries, HSG A
*	755	98	Concrete, HSG A
	186	98	Roofs, HSG A
	64,556	63	Weighted Average
	63,615		98.54% Pervious Area
	941		1.46% Impervious Area

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
16.4	50	0.0100	0.05		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.15"
1.7	70	0.0100	0.70		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
1.0	59	0.0200	0.99		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
0.0	5	0.0150	2.49		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
6.5	275	0.0100	0.70		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
0.5	50	0.0600	1.71		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps

26.1 509 Total

#### Summary for Subcatchment S202: to Porous Pavement

Runoff = 0.20 cfs @ 21.95 hrs, Volume= Routed to Pond PP : Porous Pavement 5,314 cf, Depth> 2.63"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.92"

	Area (sf)	CN	Description		
	16,526	98	Paved park	ing, HSG A	N
*	4,034	68	Open space	e, such as l	awns, parks, and cemeteries, HSG A
	128	98	Roofs, HSC	θA	
*	3,551	98	Concrete, H	ISG A	
_	24,239	93	Weighted A	verage	
	4,034		16.64% Pe	rvious Area	
	20,205		83.36% Imp	pervious Ar	ea
	Tc Length (min) (feet)	i Slop ) (ft/f	e Velocity t) (ft/sec)	Capacity (cfs)	Description
	790.0				Direct Entry, Extended TC based on 41" Section

#### Summary for Subcatchment S203: to YD-1

Runoff = 2.33 cfs @ 12.09 hrs, Volume= 7,433 cf, Depth> 3.91" Routed to Pond YD1 : YD-1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.92"

Type III 24-hr 25-Year Rainfall=5.92" Printed 4/17/2024 LC. Page 33

178 cf, Depth> 3.41"

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	A	rea (sf)	CN	Description						
*		12,383	68	Open space	e, such as l	lawns, parks, and cemeteries, HSG A				
		8,457	98	Paved park	ing, HSG A	<i>A</i>				
*		1,969	98	Concrete, H	Concrete, HSG A					
_		22.809 82 Weighted Average								
		12,383		54.29% Per	rvious Area	a				
		10,426		45.71% Imp	pervious Are	rea				
	та	l e e este	Class	Volocity	Conseitu	Description				
	IC	Length	Slope	e velocity	Capacity	Description				
_	(min)	(teet)	(ft/ft	) (ft/sec)	(cts)					
	6.0					Direct Entry,				

#### Summary for Subcatchment S204: to YD-2

Runoff	=	0.06 cfs @	12.09 hrs,	Volume=
Routed	to	Pond YD2 : YD-2		

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.92"

	Area (sf)	CN	Description	Description						
*	435	68	Open space	pen space, such as lawns, parks, and cemeteries, HSG A						
*	192	98	Concrete, H	oncrete, HSG A						
	627 435 192	77	Weighted A 69.38% Per 30.62% Imp	verage vious Area pervious Are	ea					
(m	Tc Length in) (feet)	Slop (ft/f	e Velocity t) (ft/sec)	Capacity (cfs)	Description					
6	5.0				Direct Entry.					

Direct Entry,

### Summary for Subcatchment S205: to YD-3

0.04 cfs @ 12.10 hrs, Volume= 129 cf, Depth> 2.56" Runoff = Routed to Pond YD3 : YD-3

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.92"

	Area (sf)	CN	Description						
*	605	68	Open space, such as lawns, parks, and cemeteries, HSG A						
	605		100.00% Pervious Area						
Т	c Length	Slope	e Velocity	Capacity	Description				
(mir	) (feet)	(ft/ft)	(ft/sec)	(cfs)					
6.	0				Direct Entry,				

#### Summary for Subcatchment S206: to YD-4

Runoff = 0.10 cfs @ 12.09 hrs, Volume= 322 cf, Depth> 3.51" Routed to Pond YD4 : YD-4

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.92"

	Area (sf)	CN	Description	Description					
*	728	68	Open space	e, such as la	awns, parks, and cemeteries, HSG A				
*	373	98	Concrete, H	ISG A					
	1,101 728 373	78	Weighted Average 66.12% Pervious Area 33.88% Impervious Area						
T (mir	c Length n) (feet)	Slop (ft/ft	e Velocity (ft/sec)	Capacity (cfs)	Description				
6.	0				Direct Entry,				

#### Summary for Subcatchment S207: to YD-5

186 cf. Depth> 2.93"

Runoff = 0.06 cfs @ 12.09 hrs, Volume= Routed to Pond YD5 : YD-5

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.92"

	Area (sf)	CN	Description	Description					
*	655	68	Open space	e, such as l	lawns, parks, and cemeteries, HSG A				
*	109	98	Concrete, H	oncrete, HSG A					
	764	72	Weighted A	/eighted Average					
	655		85.73% Pe	35.73% Pervious Area					
	109		14.27% Im	pervious Ar	rea				
٦	Fc Length	Slop	e Velocity	Capacity	Description				
(mi	n) (feet)	(ft/ft	:) (ft/sec)	(cfs)					
6	.0				Direct Entry,				

#### Summary for Pond DP1: Ex Site Depression

127,863 sf, 35.51% Impervious, Inflow Depth > 1.06" for 25-Year event Inflow Area = 2.13 cfs @ 12.39 hrs, Volume= Inflow 11.336 cf = 10,291 cf, Atten= 72%, Lag= 43.6 min Outflow 0.59 cfs @ 13.12 hrs, Volume= = Discarded = 0.30 cfs @ 13.12 hrs, Volume= 9,820 cf 0.28 cfs @ 13.12 hrs, Volume= 471 cf Primary = Routed to Link ap1 : AP1

Peak Elev= 262.01' @ 13.12 hrs Surf.Area= 5,447 sf Storage= 4,666 cf

Plug-Flow detention time= 194.6 min calculated for 10,291 cf (91% of inflow) Center-of-Mass det. time= 150.4 min (1,021.2 - 870.8)

Volume	Inver	t Avail.Sto	rage Storage	Description		
#1	260.00	5,97	79 cf Custom	Stage Data (Coni	<b>c)</b> Listed below (R	ecalc)
Elevatio	on S	urf.Area	Inc.Store	Cum.Store	Wet.Area	
260 (	<u>=()</u> )()	<u>(Sq-II)</u> 214			<u>(Sq-II)</u> 214	
200.0	00	2.056	978	978	2.059	
262.0	00	5,432	3,610	4,588	5,442	
262.2	25	5,700	1,391	5,979	5,718	
Device	Routing	Invert	Outlet Device	S		
#1	Discarded	260.00'	2.410 in/hr Ex	xfiltration over We	etted area Phase	e-In= 0.01'
#2	Primary	262.00'	70.0' long x	5.0' breadth Broad	d-Crested Rectang	gular Weir
			Head (feet) 0	0.20 0.40 0.60 0.8	80 1.00 1.20 1.40	0 1.60 1.80 2.00
			2.50 3.00 3.	50 4.00 4.50 5.00	0 5.50	
			Coef. (English	n) 2.34 2.50 2.70	2.68 2.68 2.66	2.65 2.65 2.65
			2.65 2.67 2.0	66 2.68 2.70 2.74	4 2.79 2.88	

**Discarded OutFlow** Max=0.30 cfs @ 13.12 hrs HW=262.01' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

Primary OutFlow Max=0.28 cfs @ 13.12 hrs HW=262.01' TW=0.00' (Dynamic Tailwater) ←2=Broad-Crested Rectangular Weir (Weir Controls 0.28 cfs @ 0.28 fps)

#### Summary for Pond PP: Porous Pavement

Inflow Area	a =	63,307 sf,	70.24% In	npervious,	Inflow Depth >	3.75"	for 25-Y	ear event
Inflow	=	4.31 cfs @	12.09 hrs,	Volume=	19,790 c	f		
Outflow	=	0.79 cfs @	12.55 hrs,	Volume=	19,774 c	f, Atten	i= 82%, L	.ag= 27.6 min
Discarded	=	0.79 cfs @	12.55 hrs,	Volume=	19,774 c	f		-
Primary	=	0.00 cfs @	0.00 hrs,	Volume=	0 c	f		
Routed	to Pond	DP1 : Ex Site	e Depressio	on				

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 261.79' @ 12.55 hrs Surf.Area= 10,986 sf Storage= 4,025 cf

Plug-Flow detention time= 24.8 min calculated for 19,774 cf (100% of inflow) Center-of-Mass det. time= 24.3 min (917.4 - 893.1)

Volume	Invert	Avail.Storage	Storage Description
#1	260.87'	13,002 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

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Elevatio (fee	on Si t)	urf.Area (sq-ft)	Void %)	s Inc.Store ) (cubic-feet)	Cum.Store (cubic-feet)
260.8	57 57	10,986	0.0	) 0	0
260.8	8	10,986	40.0	) 44	44
262.3	57	10,986	40.0	) 6,548	6,592
262.3	8	10,986	15.0	) 16	6,608
262.6	62	10,986	15.0	) 395	7,004
262.6	3	10,986	40.0	) 44	7,048
263.6	3	10,986	40.0	) 4,394	11,442
263.6	64	10,986	25.0	) 27	11,469
263.9	6	10,986	25.0	) 879	12,348
263.9	)7	10,986	15.0	) 16	12,365
264.2	9	10,986	15.0	) 527	12,892
264.3	60	10,986	100.0	) 110	13,002
Device	Routing	ln	vert	Outlet Devices	
#1	Discarded	260	.87'	2.410 in/hr Exfiltrat	ion over Surface area

			Conductivity to Groundwater Elevation = 257.75' Phase-In= 0.01'
#2	Primary	262.05'	4.0" Round Culvert X 3.00 L= 60.0' Ke= 0.500
	-		Inlet / Outlet Invert= 262.05' / 261.75' S= 0.0050 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.09 sf

**Discarded OutFlow** Max=0.79 cfs @ 12.55 hrs HW=261.79' (Free Discharge) **1=Exfiltration** (Controls 0.79 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=260.87' TW=260.00' (Dynamic Tailwater) →2=Culvert (Controls 0.00 cfs)

# Summary for Pond YD1: YD-1

Inflow Are	a =	22,809 sf,	45.71% In	npervious,	Inflow Depth >	3.91"	for 25-Year event
Inflow	=	2.33 cfs @	12.09 hrs,	Volume=	7,433 ct	F	
Outflow	=	2.33 cfs @	12.09 hrs,	Volume=	7,433 ct	f, Atten	= 0%, Lag= 0.0 min
Primary	=	2.33 cfs @	12.09 hrs,	Volume=	7,433 cf	F	
Routed	to Pond	YD2 : YD-2					

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 263.03' @ 12.09 hrs Flood Elev= 263.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	261.50'	<b>12.0" Round Culvert</b> L= 65.0' Ke= 0.500 Inlet / Outlet Invert= 261.50' / 261.18' S= 0.0049 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=2.27 cfs @ 12.09 hrs HW=262.97' TW=262.51' (Dynamic Tailwater) -1=Culvert (Outlet Controls 2.27 cfs @ 2.89 fps)

# Summary for Pond YD2: YD-2

Inflow Area = 23,436 sf, 45.31% Impervious, Inflow Depth > 3.90" for 25-Year event Inflow 2.39 cfs @ 12.09 hrs, Volume= 7.611 cf = 2.39 cfs @ 12.09 hrs, Volume= Outflow 7,611 cf, Atten= 0%, Lag= 0.0 min = Primary = 2.39 cfs @ 12.09 hrs, Volume= 7.611 cf Routed to Pond YD3 : YD-3 Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 262.55' @ 12.09 hrs Flood Elev= 263.50' Device Routing Invert Outlet Devices #1 Primary 261.18' **12.0" Round Culvert** L= 28.0' Ke= 0.500 Inlet / Outlet Invert= 261.18' / 261.04' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=2.34 cfs @ 12.09 hrs HW=262.51' TW=262.13' (Dynamic Tailwater) -1=Culvert (Inlet Controls 2.34 cfs @ 2.98 fps)

### Summary for Pond YD3: YD-3

Inflow Area	=	24,041 sf,	44.17% In	npervious,	Inflow Depth >	3.86"	for 25	-Year event
Inflow	=	2.43 cfs @	12.09 hrs,	Volume=	7,740 0	of		
Outflow	=	2.43 cfs @	12.09 hrs,	Volume=	7,740 0	of, Atte	n= 0%,	Lag= 0.0 min
Primary	=	2.43 cfs @	12.09 hrs,	Volume=	7,740 0	of		
Routed	to Pond	PP : Porous	Pavement					

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 262.15' @ 12.09 hrs Flood Elev= 263.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	261.04'	12.0" Round Culvert L= 10.0' Ke= 0.500
			Inlet / Outlet Invert= 261.04' / 260.99' S= 0.0050 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=2.38 cfs @ 12.09 hrs HW=262.13' TW=261.33' (Dynamic Tailwater) -1=Culvert (Barrel Controls 2.38 cfs @ 3.46 fps)

### Summary for Pond YD4: YD-4

Inflow Area	a =	1,101 sf,	33.88% In	npervious,	Inflow Depth >	3.51"	for 25	-Year event
Inflow	=	0.10 cfs @	12.09 hrs,	Volume=	322 c	f		
Outflow	=	0.10 cfs @	12.09 hrs,	Volume=	322 c	f, Atter	ו= 0%,	Lag= 0.0 min
Primary	=	0.10 cfs @	12.09 hrs,	Volume=	322 c	f		-
Routed	to Pond	YD5 : YD-5						

Peak Elev= 262.77' @ 12.09 hrs Flood Elev= 264.50'

DeviceRoutingInvertOutlet Devices#1Primary262.50'6.0"Round CulvertL= 39.0'Ke= 0.500Inlet / Outlet Invert=262.50'/ 262.31'S= 0.0049 '/'Cc= 0.900n=0.013Corrugated PE, smooth interior, Flow Area=0.20 sf

### Summary for Pond YD5: YD-5

Inflow Area = 1,865 sf, 25.84% Impervious, Inflow Depth > 3.27" for 25-Year event Inflow 0.16 cfs @ 12.09 hrs, Volume= 508 cf = 0.16 cfs @ 12.09 hrs, Volume= Outflow 508 cf, Atten= 0%, Lag= 0.0 min = Primary 0.16 cfs @ 12.09 hrs, Volume= = 508 cf Routed to Pond PP : Porous Pavement

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 262.61' @ 12.09 hrs Flood Elev= 264.50'

DeviceRoutingInvertOutlet Devices#1Primary262.31'6.0" Round CulvertL= 12.0'Ke= 0.500Inlet / Outlet Invert= 262.31' / 262.25'S= 0.0050 '/'Cc= 0.900n= 0.013Corrugated PE, smooth interior, Flow Area= 0.20 sf

Primary OutFlow Max=0.16 cfs @ 12.09 hrs HW=262.61' TW=261.33' (Dynamic Tailwater) -1=Culvert (Barrel Controls 0.16 cfs @ 1.85 fps)

#### Summary for Link AP1: AP1

Inflow A	rea =		127,863 sf,	35.51% In	npervious,	Inflow Depth =	= 0	.04" for	25	-Year event
Inflow	=	(	0.28 cfs @	13.12 hrs,	Volume=	471	cf			
Primary	/ =	(	0.28 cfs @	13.12 hrs,	Volume=	471	cf,	Atten= 0	%,	Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Groton 40B Post Drainage Prepared by Howard Stein Hudson Asso HydroCAD® 10.20-4a s/n 02930 © 2023 Hydr	Type III 24-hr 100-Year Rainfall=7.56"ociatesPrinted 4/17/2024oCAD Software Solutions LLCPage 39
Time span=0.00-2 Runoff by SCS TF Reach routing by Dyn-Stor-Inc	24.00 hrs, dt=0.05 hrs, 481 points x 3 2-20 method, UH=SCS, Weighted-CN I method - Pond routing by Dyn-Stor-Ind method
Subcatchment B1: Building 1 Roof	Runoff Area=6,581 sf 100.00% Impervious Runoff Depth>7.32" Tc=6.0 min CN=98 Runoff=1.09 cfs 4,012 cf
Subcatchment B2: Building 2 Roof	Runoff Area=6,581 sf 100.00% Impervious Runoff Depth>7.32" Tc=6.0 min CN=98 Runoff=1.09 cfs 4,012 cf
Subcatchment S201: to Infiltration Pond	Runoff Area=64,556 sf 1.46% Impervious Runoff Depth>3.31" ow Length=509' Tc=26.1 min CN=63 Runoff=3.42 cfs 17,790 cf
Subcatchment S202: to Porous Pavement	Runoff Area=24,239 sf 83.36% Impervious Runoff Depth>3.51" Tc=790.0 min CN=93 Runoff=0.27 cfs 7,085 cf
Subcatchment S203: to YD-1	Runoff Area=22,809 sf 45.71% Impervious Runoff Depth>5.44" Tc=6.0 min CN=82 Runoff=3.20 cfs 10,338 cf
Subcatchment S204: to YD-2	Runoff Area=627 sf 30.62% Impervious Runoff Depth>4.87" Tc=6.0 min CN=77 Runoff=0.08 cfs 254 cf
Subcatchment S205: to YD-3	Runoff Area=605 sf 0.00% Impervious Runoff Depth>3.86" Tc=6.0 min CN=68 Runoff=0.06 cfs 195 cf
Subcatchment S206: to YD-4	Runoff Area=1,101 sf 33.88% Impervious Runoff Depth>4.98" Tc=6.0 min CN=78 Runoff=0.14 cfs 457 cf
Subcatchment S207: to YD-5	Runoff Area=764 sf 14.27% Impervious Runoff Depth>4.31" Tc=6.0 min CN=72 Runoff=0.09 cfs 274 cf
Pond DP1: Ex Site Depression Discarded=0.31 cfs	Peak Elev=262.07' Storage=4,947 cf Inflow=3.48 cfs 17,975 cf 11,189 cf Primary=2.76 cfs 5,174 cf Outflow=3.06 cfs 16,363 cf
Pond PP: Porous Pavement Discarded=0.88 cf	Peak Elev=262.24' Storage=6,015 cf Inflow=5.78 cfs 26,628 cf s 26,421 cf Primary=0.11 cfs 185 cf Outflow=0.99 cfs 26,606 cf
Pond YD1: YD-1 12.0" Round	Peak Elev=264.17' Inflow=3.20 cfs 10,338 cf Culvert n=0.013 L=65.0' S=0.0049 '/' Outflow=3.20 cfs 10,338 cf
Pond YD2: YD-2 12.0" Round	Peak Elev=263.25' Inflow=3.28 cfs 10,592 cf Culvert n=0.013 L=28.0' S=0.0050 '/' Outflow=3.28 cfs 10,592 cf
Pond YD3: YD-3 12.0" Round	Peak Elev=262.50' Inflow=3.35 cfs 10,787 cf Culvert n=0.013 L=10.0' S=0.0050 '/' Outflow=3.35 cfs 10,787 cf
Pond YD4: YD-4 6.0" Rou	Peak Elev=262.83' Inflow=0.14 cfs 457 cf nd Culvert n=0.013 L=39.0' S=0.0049 '/' Outflow=0.14 cfs 457 cf
Pond YD5: YD-5 6.0" Rou	Peak Elev=262.68' Inflow=0.23 cfs 731 cf nd Culvert n=0.013 L=12.0' S=0.0050 '/' Outflow=0.23 cfs 731 cf

#### Link AP1: AP1

Inflow=2.76 cfs 5,174 cf Primary=2.76 cfs 5,174 cf

#### Total Runoff Area = 127,863 sf Runoff Volume = 44,417 cf Average Runoff Depth = 4.17" 64.49% Pervious = 82,455 sf 35.51% Impervious = 45,408 sf

4,012 cf, Depth> 7.32"

4,012 cf, Depth> 7.32"

### Summary for Subcatchment B1: Building 1 Roof

Runoff = 1.09 cfs @ 12.09 hrs, Volume= Routed to Pond PP : Porous Pavement

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=7.56"

Ar	ea (sf)	CN	Description				
	6,581	98	Roofs, HSC	θA			
	6,581		100.00% Impervious Area				
Tc (min)	Length (feet)	Slop (ft/ft	e Velocity ) (ft/sec)	Capacity (cfs)	Description		
6.0					Direct Entry,		

#### Summary for Subcatchment B2: Building 2 Roof

Runoff = 1.09 cfs @ 12.09 hrs, Volume= Routed to Pond PP : Porous Pavement

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=7.56"

Ar	rea (sf)	CN	Description				
	6,581	98	Roofs, HSG	βA			
	6,581		100.00% Impervious Area				
Tc (min)	Length (feet)	Slope (ft/ft	Velocity (ft/sec)	Capacity (cfs)	Description		
6.0					Direct Entry,		

#### Summary for Subcatchment S201: to Infiltration Pond

Runoff = 3.42 cfs @ 12.38 hrs, Volume= 17,790 cf, Depth> 3.31" Routed to Pond DP1 : Ex Site Depression

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=7.56"

	Area (sf)	CN	Description
*	13,651	43	Woods and forest that is selectively cleared, HSG A
*	49,964	68	Open space, such as lawns, parks, and cemeteries, HSG A
*	755	98	Concrete, HSG A
	186	98	Roofs, HSG A
	64,556	63	Weighted Average
	63,615		98.54% Pervious Area
	941		1.46% Impervious Area

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Type III 24-hr 100-Year Rainfall=7.56" Printed 4/17/2024 HydroCAD® 10.20-4a s/n 02930 © 2023 HydroCAD Software Solutions LLC Page 42

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
16.4	50	0.0100	0.05		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.15"
1.7	70	0.0100	0.70		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
1.0	59	0.0200	0.99		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
0.0	5	0.0150	2.49		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
6.5	275	0.0100	0.70		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
0.5	50	0.0600	1.71		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps

26.1 509 Total

#### Summary for Subcatchment S202: to Porous Pavement

0.27 cfs @ 21.95 hrs, Volume= Runoff = Routed to Pond PP : Porous Pavement

7,085 cf, Depth> 3.51"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=7.56"

	Area (sf)	CN	Description					
	16,526	98	Paved park	ing, HSG A				
*	4,034	68	Open space	e, such as l	awns, parks, and cemeteries, HSG A			
	128	98	Roofs, HSC	θA				
*	3,551	98	Concrete, H	Concrete, HSG A				
	24,239	93	Weighted Average					
	4,034		16.64% Pervious Area					
	20,205		83.36% Impervious Area					
(r	Tc Length min) (feet)	Slop (ft/f	e Velocity t) (ft/sec)	Capacity (cfs)	Description			
79	90.0				Direct Entry, Extended TC based on 41" Section			
			•					

# Summary for Subcatchment S203: to YD-1

10,338 cf, Depth> 5.44" Runoff 3.20 cfs @ 12.09 hrs, Volume= = Routed to Pond YD1 : YD-1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=7.56"

Type III 24-hr 100-Year Rainfall=7.56" Printed 4/17/2024 Page 43

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	Area (sf)	CN	Description					
*	12,383	68	Open space	e, such as l	awns, parks, and cemeteries, HSG A			
	8,457	98	Paved park	ing, HSG A	N .			
*	1,969	98	Concrete, H	Concrete, HSG A				
	22,809	82	Weighted A	Veighted Average				
	12,383		54.29% Pe	54.29% Pervious Area				
	10,426		45.71% Imp	45.71% Impervious Area				
T (mir	c Length	Slop (ft/f	e Velocity	Capacity	Description			
		(101	(1/360)	(013)				
6.	0				Direct Entry,			

#### Summary for Subcatchment S204: to YD-2

0.08 cfs @ 12.09 hrs, Volume= Runoff = Routed to Pond YD2 : YD-2

254 cf, Depth> 4.87"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=7.56"

	Area (sf)	CN	Description						
*	435	68	Open space	pen space, such as lawns, parks, and cemeteries, HSG A					
*	192	98	Concrete, H	Concrete, HSG A					
	627	77	Weighted A	Veighted Average					
	435		69.38% Pe	69.38% Pervious Area					
	192		30.62% Imp	0.62% Impervious Area					
	Tc Length	Slop	e Velocity	Capacity	Description				
(mi	in) (feet)	(ft/f	t) (ft/sec)	(cfs)					
6	6.0				Direct Entry.				

Direct Entry,

#### Summary for Subcatchment S205: to YD-3

0.06 cfs @ 12.09 hrs, Volume= 195 cf, Depth> 3.86" Runoff = Routed to Pond YD3 : YD-3

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=7.56"

	Area (sf)	CN	Description					
*	605	68	58 Open space, such as lawns, parks, and cemeteries, HSG A					
	605		100.00% Pervious Area					
Т	c Length	Slope	e Velocity	Capacity	Description			
(mir	) (feet)	(ft/ft)	(ft/sec)	(cfs)				
6.	0				Direct Entry,			

#### Summary for Subcatchment S206: to YD-4

Runoff = 0.14 cfs @ 12.09 hrs, Volume= 457 cf, Depth> 4.98" Routed to Pond YD4 : YD-4

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=7.56"

	Area (sf)	CN	Description	Description					
*	728	68	Open space	e, such as la	awns, parks, and cemeteries, HSG A				
*	373	98	Concrete, H	ISG A					
	1,101 728 373	78	Weighted A 66.12% Per 33.88% Imp	Weighted Average 36.12% Pervious Area 33.88% Impervious Area					
T (mir	c Length n) (feet)	Slop (ft/ft	e Velocity (ft/sec)	Capacity (cfs)	Description				
6.	0				Direct Entry,				

#### Summary for Subcatchment S207: to YD-5

274 cf, Depth> 4.31"

Runoff = 0.09 cfs @ 12.09 hrs, Volume= Routed to Pond YD5 : YD-5

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Type III 24-hr 100-Year Rainfall=7.56"

	Area (sf)	CN	Description					
*	655	68	Open space	e, such as l	lawns, parks, and cemeteries, HSG A			
*	109	98	Concrete, H	concrete, HSG A				
	764 655 109	72	Weighted A 85.73% Pei 14.27% Imp	Veighted Average 35.73% Pervious Area 14.27% Impervious Area				
T (mir	c Length ) (feet)	Slop (ft/f	e Velocity t) (ft/sec)	Capacity (cfs)	Description			
6.	0				Direct Entry,			

#### Summary for Pond DP1: Ex Site Depression

127,863 sf, 35.51% Impervious, Inflow Depth > 1.69" for 100-Year event Inflow Area = 3.48 cfs @ 12.39 hrs, Volume= Inflow 17,975 cf = 16,363 cf, Atten= 12%, Lag= 9.3 min Outflow 3.06 cfs @ 12.54 hrs, Volume= = Discarded = 0.31 cfs @ 12.54 hrs, Volume= 11,189 cf 2.76 cfs @ 12.54 hrs, Volume= 5,174 cf Primary = Routed to Link ap1 : AP1

Peak Elev= 262.07' @ 12.54 hrs Surf.Area= 5,502 sf Storage= 4,947 cf

Plug-Flow detention time= 141.3 min calculated for 16,329 cf (91% of inflow) Center-of-Mass det. time= 98.3 min ( 954.9 - 856.6 )

Volume	Inver	t Avail.Sto	rage Storage	Description		
#1	260.00	5,97	79 cf Custon	n Stage Data (Con	<b>ic)</b> Listed below (F	Recalc)
Elevatio	on S	urf.Area	Inc.Store	Cum.Store	Wet.Area	
(tee	et)	(sq-tt)	(CUDIC-TEET)	(CUDIC-TEET)	(sq-tt)	
260.0	00	214	0	0	214	
261.0	00	2,056	978	978	2,059	
262.0	00	5,432	3,610	4,588	5,442	
262.2	25	5,700	1,391	5,979	5,718	
Device	Routing	Invert	Outlet Device	es		
#1	Discarded	260.00'	2.410 in/hr E	xfiltration over We	etted area Phas	se-In= 0.01'
#2 Primary		262.00'	70.0' long x	5.0' breadth Broad	d-Crested Rectan	igular Weir
	-		Head (feet)	0.20 0.40 0.60 0.	80 1.00 1.20 1.4	10 1.60 1.80 2.00
			2.50 3.00 3.	50 4.00 4.50 5.0	0 5.50	
			Coef. (Englis	h) 2.34 2.50 2.70	2.68 2.68 2.66	2.65 2.65 2.65
			2.65 2.67 2.	66 2.68 2.70 2.7	4 2.79 2.88	

**Discarded OutFlow** Max=0.31 cfs @ 12.54 hrs HW=262.07' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.31 cfs)

Primary OutFlow Max=2.73 cfs @ 12.54 hrs HW=262.07' TW=0.00' (Dynamic Tailwater) ←2=Broad-Crested Rectangular Weir (Weir Controls 2.73 cfs @ 0.60 fps)

#### Summary for Pond PP: Porous Pavement

Inflow Area	a =	63,307 sf,	70.24% In	npervious,	Inflow Depth >	5.05"	for 100	-Year event
Inflow	=	5.78 cfs @	12.09 hrs,	Volume=	26,628 c	f		
Outflow	=	0.99 cfs @	12.57 hrs,	Volume=	26,606 c	f, Atten	= 83%,	Lag= 28.7 min
Discarded	=	0.88 cfs @	12.56 hrs,	Volume=	26,421 c	f		-
Primary	=	0.11 cfs @	12.57 hrs,	Volume=	185 c	f		
Routed to Pond DP1 : Ex Site Depression								

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 262.24' @ 12.56 hrs Surf.Area= 10,986 sf Storage= 6,015 cf

Plug-Flow detention time= 37.2 min calculated for 26,551 cf (100% of inflow) Center-of-Mass det. time= 36.7 min (923.4 - 886.7)

Volume	Invert	Avail.Storage	Storage Description
#1	260.87'	13,002 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
Phase-In= 0.01'

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Elevatio (fee	n Sı t)	urf.Area (sq-ft)	Voids %)	s Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
260.8	57	10,986	0.0	) 0	0	
260.8	8	10,986	40.0	) 44	44	
262.3	57	10,986	40.0	6,548	6,592	
262.3	8	10,986	15.0	) 16	6,608	
262.6	2	10,986	15.0	) 395	7,004	
262.6	3	10,986	40.0	) 44	7,048	
263.6	3	10,986	40.0	) 4,394	11,442	
263.6	4	10,986	25.0	) 27	11,469	
263.9	6	10,986	25.0	) 879	12,348	
263.9	7	10,986	15.0	) 16	12,365	
264.2	9	10,986	15.0	) 527	12,892	
264.3	0	10,986	100.0	) 110	13,002	
Device	Routing	In	vert	Outlet Devices		
#1	Discarded	260	.87'	2.410 in/hr Exfiltrat	ion over Surface	area
				Conductivity to Grou	undwater Elevatio	n = 257.75'

#2 Primary 262.05' **4.0'' Round Culvert X 3.00** L= 60.0' Ke= 0.500 Inlet / Outlet Invert= 262.05' / 261.75' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.09 sf

**Discarded OutFlow** Max=0.88 cfs @ 12.56 hrs HW=262.24' (Free Discharge) **1=Exfiltration** (Controls 0.88 cfs)

**Primary OutFlow** Max=0.11 cfs @ 12.57 hrs HW=262.24' TW=262.06' (Dynamic Tailwater) **2=Culvert** (Outlet Controls 0.11 cfs @ 1.01 fps)

#### Summary for Pond YD1: YD-1

 Inflow Area =
 22,809 sf, 45.71% Impervious, Inflow Depth > 5.44" for 100-Year event

 Inflow =
 3.20 cfs @
 12.09 hrs, Volume=
 10,338 cf

 Outflow =
 3.20 cfs @
 12.09 hrs, Volume=
 10,338 cf, Atten= 0%, Lag= 0.0 min

 Primary =
 3.20 cfs @
 12.09 hrs, Volume=
 10,338 cf

 Routed to Pond YD2 : YD-2
 10.338 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 264.17' @ 12.09 hrs Flood Elev= 263.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	261.50'	<b>12.0" Round Culvert</b> L= 65.0' Ke= 0.500 Inlet / Outlet Invert= 261.50' / 261.18' S= 0.0049 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=3.13 cfs @ 12.09 hrs HW=264.07' TW=263.20' (Dynamic Tailwater) -1=Culvert (Outlet Controls 3.13 cfs @ 3.99 fps)

#### Summary for Pond YD2: YD-2

Inflow Area = 23,436 sf, 45.31% Impervious, Inflow Depth > 5.42" for 100-Year event Inflow 3.28 cfs @ 12.09 hrs, Volume= 10.592 cf = 3.28 cfs @ 12.09 hrs, Volume= Outflow 10,592 cf, Atten= 0%, Lag= 0.0 min = Primary = 3.28 cfs @ 12.09 hrs, Volume= 10.592 cf Routed to Pond YD3 : YD-3 Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 263.25' @ 12.09 hrs Flood Elev= 263.50' Device Routing Invert Outlet Devices #1 Primary 261.18' **12.0" Round Culvert** L= 28.0' Ke= 0.500 Inlet / Outlet Invert= 261.18' / 261.04' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=3.21 cfs @ 12.09 hrs HW=263.20' TW=262.48' (Dynamic Tailwater) **1=Culvert** (Inlet Controls 3.21 cfs @ 4.09 fps)

#### Summary for Pond YD3: YD-3

Inflow Area	=	24,041 sf,	44.17% In	npervious,	Inflow Depth >	5	.38" fo	r 10	0-Year even	t
Inflow	=	3.35 cfs @	12.09 hrs,	Volume=	10,787	cf				
Outflow	=	3.35 cfs @	12.09 hrs,	Volume=	10,787	cf,	Atten= (	)%,	Lag= 0.0 mir	ſ
Primary	=	3.35 cfs @	12.09 hrs,	Volume=	10,787	cf			-	
Routed	to Pond	PP : Porous	Pavement							

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 262.50' @ 12.09 hrs Flood Elev= 263.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	261.04'	12.0" Round Culvert L= 10.0' Ke= 0.500
			Inlet / Outlet Invert= 261.04' / 260.99' S= 0.0050 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

**Primary OutFlow** Max=3.27 cfs @ 12.09 hrs HW=262.48' TW=261.57' (Dynamic Tailwater) **1=Culvert** (Barrel Controls 3.27 cfs @ 4.16 fps)

#### Summary for Pond YD4: YD-4

Inflow Are	a =	1,101 sf,	33.88% In	npervious,	Inflow Depth >	4.98"	for 10	0-Year event
Inflow	=	0.14 cfs @	12.09 hrs,	Volume=	457 c	f		
Outflow	=	0.14 cfs @	12.09 hrs,	Volume=	457 c	f, Atte	n= 0%,	Lag= 0.0 min
Primary	=	0.14 cfs @	12.09 hrs,	Volume=	457 c	f		-
Routed	to Pond	YD5 : YD-5						

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 262.83' @ 12.09 hrs Flood Elev= 264.50'

DeviceRoutingInvertOutlet Devices#1Primary262.50'6.0"Round CulvertL= 39.0'Ke= 0.500Inlet / Outlet Invert=262.50'/ 262.31'S= 0.0049 '/'Cc= 0.900n= 0.013Corrugated PE, smooth interior, Flow Area=0.20 sf

#### Summary for Pond YD5: YD-5

Inflow Area =1,865 sf, 25.84% Impervious, Inflow Depth > 4.71" for 100-Year eventInflow =0.23 cfs @12.09 hrs, Volume=731 cfOutflow =0.23 cfs @12.09 hrs, Volume=731 cf, Atten= 0%, Lag= 0.0 minPrimary =0.23 cfs @12.09 hrs, Volume=731 cfRouted to Pond PP : Porous Pavement731 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 262.68' @ 12.09 hrs Flood Elev= 264.50'

DeviceRoutingInvertOutlet Devices#1Primary262.31'6.0" Round CulvertL= 12.0'Ke= 0.500Inlet / Outlet Invert= 262.31' / 262.25'S= 0.0050 '/'Cc= 0.900n= 0.013Corrugated PE, smooth interior, Flow Area= 0.20 sf

Primary OutFlow Max=0.23 cfs @ 12.09 hrs HW=262.68' TW=261.58' (Dynamic Tailwater) -1=Culvert (Barrel Controls 0.23 cfs @ 2.03 fps)

#### Summary for Link AP1: AP1

Inflow A	Area =	127,863 sf,	35.51% Im	npervious,	Inflow Depth =	0.49"	for 10	0-Year event
Inflow	=	2.76 cfs @	12.54 hrs,	Volume=	5,174 c	f		
Primary	/ =	2.76 cfs @	12.54 hrs,	Volume=	5,174 c	f, Atte	en= 0%,	Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

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# Stage-Area-Storage for Pond DP1: Ex Site Depression

Elevation	Surface	Wetted	Storage
(feet)	(sq-ft)	(sq-ft)	(cubic-feet)
260.00	214	214	0
260.05	261	261	12
260.10	313	313	26
260.15	370	370	43
260.20	431	432	63
260.25	498	498	80
200.30	00C 644	509 645	113
260.33	724	725	143
260.40	809	810	216
260.50	899	900	259
260.55	994	995	306
260.60	1,093	1,094	358
260.65	1,197	1,198	415
260.70	1,305	1,307	478
260.75	1,419	1,421	546
260.80	1,537	1,539	620
260.85	1,659	1,662	700
260.90	1,787	1,790	786
260.95	1,919	1,922	878
261.00	2,056	2,059	978
261.05	2,187	2,190	1,084
261.10	2,321	2,325	1,196
201.15	2,400	2,404	1,310
261.20	2,000	2,007	1,440
261.20	2,740	2,704	1,370
261.35	3.055	3.060	1,866
261.40	3,213	3,219	2,023
261.45	3,376	3,382	2,188
261.50	3,543	3,549	2,361
261.55	3,714	3,720	2,542
261.60	3,889	3,895	2,732
261.65	4,067	4,074	2,931
261.70	4,250	4,258	3,139
261.75	4,437	4,445	3,356
261.80	4,628	4,636	3,583
261.85	4,823	4,832	3,819
201.90	5,022	5,031	4,000
201.95	5,225	5,234	4,321
262.00	5 485	5 496	4,000
262.10	5,538	5,551	5,136
262.15	5.592	5.606	5.415
262.20	5,646	5,662	5,695
262.25	5,700	5,718	5,979

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# Stage-Area-Storage for Pond PP: Porous Pavement

Elevation (feet)	Surface (sg-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
260.87	10 986	0	263.47	10 986	10 739
260.07	10,986	220	263 52	10,000	10,755
260.02	10,000	430	263.57	10,000	11 178
261.02	10,000	659	263.62	10,000	11 308
261.02	10,000	870	263.67	10,000	11,550
261.07	10,900	1 000	263.07	10,900	11,552
261.12	10,300	1,055	263.72	10,900	11,003
261.17	10,300	1,510	263.82	10,900	11,020
261.22	10,000	1,000	263.87	10,000	12 101
261.27	10,000	1,700	263.92	10,986	12,101
261.32	10,000	2 197	263.92	10,000	12,200
261.07	10,000	2,107	264.02	10,986	12,000
261.42	10,000	2,417	264.02	10,986	12,447
261.52	10,000	2,856	264 12	10,986	12,000
261.52	10,000	3 076	264.12	10,986	12,612
261.62	10,000	3 296	264 22	10,986	12,001
261.62	10,986	3 516	264.27	10,986	12,859
261.72	10,986	3,735	201121	10,000	,
261.77	10,986	3,955			
261.82	10,986	4,175			
261.87	10,986	4.394			
261.92	10,986	4.614			
261.97	10,986	4.834			
262.02	10,986	5.054			
262.07	10,986	5,273			
262.12	10,986	5,493			
262.17	10,986	5,713			
262.22	10,986	5,932			
262.27	10,986	6,152			
262.32	10,986	6,372			
262.37	10,986	6,592			
262.42	10,986	6,674			
262.47	10,986	6,756			
262.52	10,986	6,839			
262.57	10,986	6,921			
262.62	10,986	7,004			
262.67	10,986	7,223			
262.72	10,986	7,443			
262.77	10,986	7,663			
262.82	10,986	7,882			
262.87	10,986	8,102			
262.92	10,986	8,322			
262.97	10,986	8,542			
263.02	10,986	8,761			
263.07	10,986	8,981			
263.12	10,986	9,201			
263.17	10,986	9,420			
263.22	10,986	9,640			
263.27	10,986	9,860			
263.32	10,986	10,080			
263.37	10,986	10,299			
263.42	10,986	10,519			

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# Stage-Area-Storage for Pond YD1: YD-1

Elevation (feet)	Storage (cubic-feet)	Elevation (feet)	Storage (cubic-feet)	Elevation (feet)	Storage (cubic-feet)
261.50	Ó	262.54	0	263.58	0
261.52	0	262.56	0	263.60	0
261.54	0	262.58	0	263.62	0
261.56	0	262.60	0	263.64	0
261.58	0	262.62	0	263.66	0
261.60	0	262.64	0	263.68	0
261.62	0	262.66	0	263.70	0
261.64	0	262.68	0	263.72	0
261.66	0	262.70	0	263.74	0
261.68	0	262.72	0	263.76	0
261.70	0	262.74	0	263.78	0
261.72	0	262.76	0	263.80	0
261.74	0	262.78	0	263.82	0
261.76	0	262.80	0	263.84	0
261.78	0	262.82	0	263.86	0
201.80	0	202.84	0	203.88	0
201.02	0	202.00	0	203.90	0
201.04	0	202.00	0	203.92	0
261.88	0	262.90	0	263.94	0
261.00	0	262.02	0	263.00	0
261.92	0	262.94	0	264.00	0
261.94	0	262.98	0	264.00	0
261.96	Ő	263.00	Õ	264.04	0
261.98	Ő	263.02	0	264.06	0
262.00	0	263.04	0	264.08	0
262.02	0	263.06	0	264.10	0
262.04	0	263.08	0	264.12	0
262.06	0	263.10	0	264.14	0
262.08	0	263.12	0	264.16	0
262.10	0	263.14	0		
262.12	0	263.16	0		
262.14	0	263.18	0		
262.16	0	263.20	0		
262.18	0	263.22	0		
262.20	0	263.24	0		
262.22	0	263.26	0		
202.24	0	203.20	0		
202.20	0	203.30	0		
202.20	0	203.32	0		
262.30	0	263.34	0		
262.32	0	263.38	0		
262.36	0	263.40	Ő		
262.38	Ő	263.42	Õ		
262.40	0 0	263.44	0		
262.42	Ő	263.46	0		
262.44	0	263.48	Ó		
262.46	0	263.50	Ó		
262.48	0	263.52	0		
262.50	0	263.54	0		
262.52	0	263.56	0		

262.20

0

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Elevation Storage Elevation Storage Elevation Storage (feet) (cubic-feet) (feet) (cubic-feet) (feet) (cubic-feet) 261.18 262.22 263.26 0 0 261.20 0 262.24 0 263.28 0 0 0 261.22 262.26 0 263.30 0 0 0 261.24 262.28 263.32 0 0 0 261.26 262.30 263.34 261.28 0 262.32 0 263.36 0 261.30 0 262.34 0 263.38 0 261.32 0 262.36 0 263.40 0 261.34 0 262.38 0 263.42 0 261.36 0 262.40 0 263.44 0 0 261.38 0 262.42 0 263.46 262.44 0 0 261.40 0 263.48 261.42 0 262.46 0 263.50 0 0 262.48 0 261.44 0 0 261.46 262.50 261.48 0 262.52 0 261.50 0 0 262.54 0 261.52 0 262.56 0 0 261.54 262.58 261.56 0 0 262.60 0 0 261.58 262.62 261.60 0 262.64 0 0 0 261.62 262.66 261.64 0 262.68 0 261.66 0 0 262.70 261.68 0 0 262.72 261.70 0 262.74 0 261.72 0 262.76 0 261.74 0 0 262.78 0 0 261.76 262.80 261.78 0 0 262.82 0 261.80 0 262.84 261.82 0 262.86 0 262.88 0 261.84 0 261.86 0 262.90 0 0 0 261.88 262.92 0 0 261.90 262.94 0 261.92 0 262.96 261.94 0 0 262.98 261.96 0 263.00 0 0 0 261.98 263.02 0 262.00 263.04 0 0 0 262.02 263.06 262.04 0 263.08 0 262.06 0 263.10 0 262.08 0 263.12 0 262.10 0 263.14 0 0 262.12 263.16 0 0 262.14 0 263.18 262.16 0 263.20 0 0 262.18 0 263.22 0 0

263.24

#### Stage-Area-Storage for Pond YD2: YD-2

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# Stage-Area-Storage for Pond YD3: YD-3

Elevation (feet)	Storage (cubic-feet)	Elevation (feet)	Storage (cubic-feet)	Elevation (feet)	Storage (cubic-feet)
261.04	0	262.08		263.12	
261.06	0	262.10	0	263.14	0
261.08	0	262.12	0	263.16	0
261.10	0	262.14	0	263.18	0
261 12	0 0	262 16	0 0	263 20	0 0
261 14	Õ	262.18	Õ	263.22	Õ
261.16	Õ	262.20	0 0	263.24	0 0
261.10	Õ	262.20	Õ	263.26	Õ
261.20	Õ	262.24	Õ	263.28	Õ
261.22	Õ	262.26	0 0	263.30	0 0
261.22	0 0	262.28	Õ	263.32	Õ
261.21	0 0	262.20	Õ	263.34	ů 0
261.20	0	262.32	0	263.36	0
261.20	Õ	262.34	Õ	263.38	Õ
261.32	0	262.36	0	263.40	0
261.32	0	262.38	0	263.40	0
261.34	0	262.00	0	263.42	0
261.38	0	262.40	0	263.44	0
261.00	0	262.42	0	263.48	0
261.40	0	262.44	0	263 50	0
261.42	0	262.40	0	200.00	Ŭ
261.44	0	262.40	0		
261.40	0	262.50	0		
261.40	0	262.52	0		
261.50	0	262.54	0		
261.52	0	262.58	0		
261.54	0	262.60	0		
261.58	0	262.00	0		
261.60	0	262.62	0		
261.60	0	262.64	0		
261.62	0	262.68	0		
261.64	0	262.00	0		
261.68	0	262.70	0		
261.00	Õ	262.72	Õ		
261.72	Õ	262.76	0 0		
261.72	Õ	262.78	Õ		
261.76	0 0	262.80	Õ		
261.78	Õ	262.80	Õ		
261.80	0 0	262.84	Õ		
261.82	Õ	262.86	Õ		
261.84	0 0	262.88	Õ		
261.86	Õ	262.90	Õ		
261.88	0 0	262.92	Õ		
261.90	0 0	262.94	0 0		
261.92	0 0	262.96	Õ		
261.94	0	262.98	0		
261.96	0	263.00	0		
261.98	0 0	263.02	Ő		
262.00	0	263.04	0		
262.02	0	263.06	0		
262.04	0	263.08	0		
262.06	Ő	263.10	Ő		
	-		-		

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#### Stage-Area-Storage for Pond YD4: YD-4

Elevation	Storage	Elevation	Storage
(feet)	(cubic-feet)	(feet)	(cubic-feet)
262.50	0	263.54	0
262.52	0	263.56	0
262.54	0	263.58	0
202.00	0	203.00	0
202.00	0	203.02	0
262.00	0	263.66	0
262.62	0	263.68	0
262.66	0 0	263.70	0 0
262.68	0	263.72	0
262.70	0	263.74	0
262.72	0	263.76	0
262.74	0	263.78	0
262.76	0	263.80	0
262.78	0	263.82	0
262.80	0	263.84	0
262.82	0	203.80	0
202.04	0	203.00	0
262.88	0	263.90	0
262.90	0 0	263.94	0
262.92	0	263.96	Ő
262.94	0	263.98	0
262.96	0	264.00	0
262.98	0	264.02	0
263.00	0	264.04	0
263.02	0	264.06	0
263.04	0	264.08	0
203.00	0	204.10	0
203.00	0	204.12	0
263.10	0	264.14	0
263.14	ů 0	264.18	Ő
263.16	0	264.20	0
263.18	0	264.22	0
263.20	0	264.24	0
263.22	0	264.26	0
263.24	0	264.28	0
263.26	0	264.30	0
263.28	0	264.32	0
263.30	0	264.34	0
203.32	0	204.30	0
263.36	0	264.30	0
263.38	0	264.42	0 0
263.40	0	264.44	0 0
263.42	0	264.46	0
263.44	0	264.48	0
263.46	0	264.50	0
263.48	0		
263.50	0		
203.52	U		
		l	

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Stage-Area-Storage for Pond YD5: YD-5

Elevation	Storage	Elevation	Storage	Elevation	Storage
(feet)	(cubic-feet)	(feet)	(cubic-feet)	(feet)	(cubic-feet)
262.31	0	263.35	0	264.39	0
262.33	0	263.37	0	264.41	0
262.35	0	263.39	0	264.43	0
262.37	0	263.41	0	264.45	0
262.39	0	263.43	0	264.47	0
262.41	0	263.45	0	264.49	0
262.43	0	263.47	0		
262.45	0	263.49	0		
262.47	0	263.51	0		
262.49	0	263.53	0		
262.51	0	263.55	0		
262.53	0	263.57	0		
262.55	0	263.59	0		
262.57	0	263.61	0		
262.59	0	263.63	0		
262.61	0	263.65	0		
262.63	0	263.67	0		
262.65	0	263.69	0		
262.67	0	263.71	0		
262.69	0	263.73	0		
262.71	0	263.75	0		
262.73	0	263.77	0		
262.75	0	263.79	0		
262.77	0	263.81	0		
262.79	0	263.83	0		
262.81	0	263.85	0		
262.83	0	263.87	0		
262.85	0	263.89	0		
262.87	0	263.91	0		
262.89	0	263.93	0		
262.91	0	263.95	0		
262.93	0	263.97	0		
262.95	0	263.99	0		
262.97	0	264.01	0		
262.99	0	264.03	0		
263.01	0	264.05	0		
263.03	0	264.07	0		
263.05	0	264.09	0		
263.07	0	264.11	0		
263.09	0	264.13	0		
263.11	0	264.15	0		
263.13	0	264.17	0		
263.15	0	264.19	0		
263.17	0	264.21	0		
263.19	0	264.23	0		
263.21	0	264.25	0		
263.23	0	264.27	0		
263.25	0	264.29	0		
263.27	0	264.31	0		
263.29	0	264.33	0		
263.31	0	264.35	0		
263.33	0	264.37	0		